

1.50

$$a) \vec{F}_1(\vec{r}) = x^2 \hat{z}$$

$$\vec{F}_2(\vec{r}) = x \hat{x} + y \hat{y} + z \hat{z}$$

$$\vec{\nabla} \cdot \vec{F}_1 = \frac{\partial F_{1x}}{\partial x} + \frac{\partial F_{1y}}{\partial y} + \frac{\partial F_{1z}}{\partial z} = 0$$

$$\begin{aligned} \vec{\nabla} \times \vec{F}_1 &= \hat{x} \left(\frac{\partial F_{1z}}{\partial y} - \frac{\partial F_{1y}}{\partial z} \right) + \hat{y} \left(\frac{\partial F_{1x}}{\partial z} - \frac{\partial F_{1z}}{\partial x} \right) + \hat{z} \left(\frac{\partial F_{1y}}{\partial x} - \frac{\partial F_{1x}}{\partial y} \right) \\ &= 0 + (-2x \hat{y}) + 0 = -2x \hat{y} \end{aligned}$$

$$\vec{\nabla} \cdot \vec{F}_2 = \frac{\partial F_{2x}}{\partial x} + \frac{\partial F_{2y}}{\partial y} + \frac{\partial F_{2z}}{\partial z} = \frac{\partial x}{\partial x} + \frac{\partial y}{\partial y} + \frac{\partial z}{\partial z} = 1 + 1 + 1 = 3$$

$$\vec{\nabla} \times \vec{F}_2 = 0$$

so we can write $\vec{F}_1 = \vec{\nabla} \times \vec{W}$ and $\vec{F}_2 = -\vec{\nabla} U$

To find \vec{W} we want $\frac{\partial W_y}{\partial x} - \frac{\partial W_x}{\partial y} = x^2$

choose $\vec{W} = \frac{1}{3} x^3 \hat{y}$

then $\vec{\nabla} \times \vec{W} = \hat{x} \left(\frac{\partial W_z}{\partial y} - \frac{\partial W_y}{\partial z} \right)$

$$+ \hat{y} \left(\frac{\partial W_x}{\partial z} - \frac{\partial W_z}{\partial x} \right) + \hat{z} \left(\frac{\partial W_y}{\partial x} - \frac{\partial W_x}{\partial y} \right)$$

$$= 0 + 0 + \hat{z} (x^2 - 0) = x^2 \hat{z} = \vec{F}_1$$

To find $U(\vec{r})$ we can take

$$U(\vec{r}) = - \int_{\vec{r}_0}^{\vec{r}} d\vec{q} \cdot \vec{F}_2$$

where it does not matter what we choose for the point \vec{r}_0 , or the path we take from \vec{r}_0 to \vec{r} (since $\vec{\nabla} \times \vec{F}_2 = 0$)

Choose $\vec{r}_0 = 0$, and choose the path to go in a straight line from the origin to the point \vec{r} .

We can parameterize the path as $\vec{r}'(t) = (xt)\hat{x} + (yt)\hat{y} + (zt)\hat{z}$ with t going from 0 to 1

$$\text{Then } U(\vec{r}) = - \int_0^1 dt \frac{d\vec{r}'(t)}{dt} \cdot \vec{F}_2(\vec{r}'(t))$$

$$= - \int_0^1 dt (x\hat{x} + y\hat{y} + z\hat{z}) \cdot (xt\hat{x} + yt\hat{y} + zt\hat{z})$$

$$= - \int_0^1 dt (x^2 + y^2 + z^2)t = -\frac{1}{2}(x^2 + y^2 + z^2)$$

$$\text{So } \boxed{U(\vec{r}) = -\frac{1}{2}r^2} \quad \text{since } \int_0^1 dt t = \frac{1}{2}$$

$$\text{Check } -\vec{\nabla}(-\frac{1}{2}r^2) = \frac{1}{2}\vec{\nabla}(x^2 + y^2 + z^2)$$

$$= \frac{1}{2}(2x\hat{x} + 2y\hat{y} + 2z\hat{z})$$

$$= x\hat{x} + y\hat{y} + z\hat{z} = \vec{F}_2$$

$$b) \vec{F}_3 = yz \hat{x} + zx \hat{y} + xy \hat{z}$$

Shows we can write both $\vec{F}_3 = -\vec{\nabla}U$ and $\vec{F}_3 = \vec{\nabla} \times \vec{W}$

$$\vec{\nabla} \cdot \vec{F}_3 = \frac{\partial F_{3x}}{\partial x} + \frac{\partial F_{3y}}{\partial y} + \frac{\partial F_{3z}}{\partial z} = 0$$

$$\begin{aligned} \vec{\nabla} \times \vec{F}_3 &= \hat{x} \left(\frac{\partial F_{3z}}{\partial y} - \frac{\partial F_{3y}}{\partial z} \right) + \hat{y} \left(\frac{\partial F_{3x}}{\partial z} - \frac{\partial F_{3z}}{\partial x} \right) + \hat{z} \left(\frac{\partial F_{3y}}{\partial x} - \frac{\partial F_{3x}}{\partial y} \right) \\ &= \hat{x} (x - x) + \hat{y} (y - y) + \hat{z} (z - z) = 0 \end{aligned}$$

since $\vec{\nabla} \cdot \vec{F}_3 = 0$ we can write $\vec{F}_3 = \vec{\nabla} \times \vec{W}$

since $\vec{\nabla} \times \vec{F}_3 = 0$ we can write $\vec{F}_3 = -\vec{\nabla}U$

To find \vec{W} we want

$$\frac{\partial W_z}{\partial y} - \frac{\partial W_y}{\partial z} = F_{3x} = yz$$

$$\frac{\partial W_x}{\partial z} - \frac{\partial W_z}{\partial x} = F_{3y} = zx$$

$$\frac{\partial W_y}{\partial x} - \frac{\partial W_x}{\partial y} = F_{3z} = xy$$

$$\text{Try } W_z = \frac{1}{2} y^2 z, \quad W_x = \frac{1}{2} z^2 x, \quad W_y = \frac{1}{2} x^2 y$$

$$\vec{W} = \frac{1}{2} (z^2 x \hat{x} + x^2 y \hat{y} + y^2 z \hat{z})$$

$$\text{can verify that } \vec{\nabla} \times \vec{W} = (yz) \hat{x} + (zx) \hat{y} + (xy) \hat{z} = \vec{F}_3$$

To find U we can do $U(\vec{r}) = -\int_{r_0}^{\vec{r}} d\vec{l} \cdot \vec{F}_3$ or
can try a more direct approach

$$\frac{\partial U}{\partial x} = -F_{3x} = yz$$

$$\frac{\partial U}{\partial y} = -F_{3y} = zx$$

$$\frac{\partial U}{\partial z} = -F_{3z} = xy$$

Try $\boxed{U(\vec{r}) = -xyz}$

can verify that $-\vec{\nabla}U = \vec{F}_3$

2.9 | $\vec{E}(\vec{r}) = kr^3 \hat{r}$ in spherical coordinates

a) Find charge density $\rho(\vec{r})$

$$\text{We know } \vec{\nabla} \cdot \vec{E} = \rho/\epsilon_0$$

evaluate $\vec{\nabla} \cdot \vec{E}$ in spherical coordinates. Since \vec{E} points in radial direction and depends only on the radial coordinate, only the radial term in $\vec{\nabla} \cdot \vec{E}$ is not zero.

$$\begin{aligned} \text{So } \vec{\nabla} \cdot \vec{E} &= \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 E(r)) = \frac{k}{r^2} \frac{\partial}{\partial r} (r^5) \\ &= \frac{5k}{r^2} r^4 = 5kr^2 = \rho/\epsilon_0 \end{aligned}$$

$$\boxed{\rho(\vec{r}) = 5\epsilon_0 k r^2}$$

b) Charge within sphere of radius R centered at origin

$$i) Q = \int_0^R dr r^2 \int_0^\pi d\theta \sin\theta \int_0^{2\pi} d\varphi \rho(\vec{r})$$

volume integral in spherical coordinates

$$\begin{aligned} &= 4\pi \int_0^R dr r^2 \rho(r) = (4\pi)(5\epsilon_0 k) \int_0^R dr r^2 (r^2) \\ &= (4\pi)(5\epsilon_0 k) \frac{R^5}{5} = \boxed{4\pi\epsilon_0 k R^5 = Q} \end{aligned}$$

or from Gauss' law

$$2) \frac{Q}{\epsilon_0} = \oint_S d\vec{a} \cdot \vec{E}$$

where S is the surface
of the sphere of radius R .

$$= \int_0^\pi d\theta \int_0^{2\pi} d\phi \sin\theta R^2 \hat{r} \cdot (kR^3 \hat{r})$$

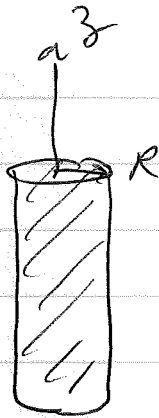
↑ since evaluating \vec{E} at $r=R$

$$= (4\pi) k R^5$$

↑ from angular integrations

$$Q = 4\pi \epsilon_0 k R^5$$

2.13/ but more general



uniform charge density ρ inside
infinitely long cylindrical wire of
radius R . Charge per unit length is λ

$$\text{so } \lambda = \pi R^2 \rho$$

Find \vec{E} inside and outside the cylinder using Gauss' law.

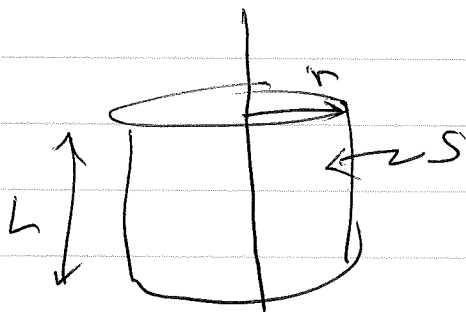
1) Integral method

~~By symmetry of rotational invariance about \hat{z}
 $\vec{E}(r)$ must have the form $E(r)\hat{r}$ where
 r is the cylindrical radial direction~~

Because of rotational symmetry about the z axis, \vec{E} cannot involve polar angle φ

Because of translational symmetry along \hat{z} axis, \vec{E} cannot involve the coordinate z .

$\Rightarrow \vec{E}(r)$ must have the form $E(r)\hat{r}$ where
here r is the cylindrical radial direction
 \hat{r} is the corresponding cylindrical radial
unit vector



evaluate $\oint_S d\vec{a} \cdot \vec{E}$ on a

cylindrical surface of radius r
and length L .

Since \vec{E} is in the \hat{r} direction there is no contribution from top and bottom surfaces, since $\hat{r} \cdot \vec{E} = 0$

$$\oint_S d\vec{a} \cdot \vec{E} = \int_0^L dz \int_0^{2\pi} d\phi \int r \hat{r} \cdot \vec{E} = L 2\pi r E(r) = \frac{Q_{\text{encl}}}{\epsilon_0}$$

Now if $r > R$, then $Q_{\text{encl}} = L\lambda$ so

$$\boxed{\vec{E}(\vec{r}) = \frac{\lambda}{2\pi\epsilon_0 r} \hat{r} \quad r > R}$$

If $r < R$ then

$$\begin{aligned} Q_{\text{encl}} &= \int_0^L dz \int_0^{2\pi} d\phi \int_0^r dr' r' \rho = (L)(2\pi) \frac{r^2}{2} \rho = L\pi r^2 \rho \\ &= L\lambda \frac{r^2}{R^2} \quad \text{using } \lambda = \pi R^2 \rho \end{aligned}$$

$$\text{so } L 2\pi r E(r) = \frac{L\lambda r^2}{\epsilon_0 R^2}$$

$$\boxed{\vec{E}(\vec{r}) = \frac{\lambda}{2\pi\epsilon_0} \frac{r}{R^2} \hat{r} \quad r < R}$$

2) Solve using Gauss' Law in differential form

$$\vec{\nabla} \cdot \vec{E} = \rho / \epsilon_0 \quad \text{with} \quad \vec{E}(\vec{r}) = E(r) \hat{r}$$

evaluate divergence in cylindrical coordinates

$$\vec{\nabla} \cdot \vec{E} = \frac{1}{r} \frac{\partial}{\partial r} (rE) = \frac{\rho(r)}{\epsilon_0} \quad \rho(r) = \begin{cases} \rho & r < R \\ 0 & r > R \end{cases}$$

$$\frac{\partial}{\partial r} (rE) = \frac{r \rho(r)}{\epsilon_0}$$

integrate from $r' = 0$ to $r' = r$

$$rE(r) - 0 = \frac{1}{\epsilon_0} \int_0^r dr' r' \rho(r')$$

$$= \begin{cases} \frac{1}{\epsilon_0} \frac{1}{2} R^2 \rho & \text{for } r > R \\ \frac{1}{\epsilon_0} \frac{1}{2} r^2 \rho & \text{for } r < R \end{cases}$$

$$E(r) = \begin{cases} \frac{R^2 \rho}{2 \epsilon_0 r} & \text{for } r > R \\ \frac{r \rho}{2 \epsilon_0} & \text{for } r < R \end{cases}$$

$$\lambda = \pi R^2 \rho \quad \text{so} \quad \rho = \frac{\lambda}{\pi R^2} \quad \text{substitute in}$$

$$\vec{E}(\vec{r}) = \begin{cases} \frac{\lambda}{2\pi\epsilon_0 r} \hat{r} & r > R \\ \frac{\lambda}{2\pi\epsilon_0} \frac{r}{R^2} \hat{r} & r < R \end{cases}$$