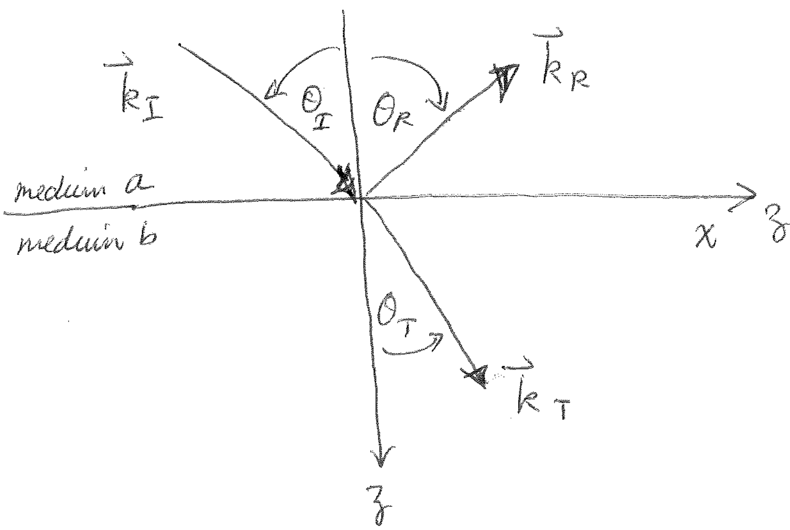
Reflection and Transmission (Refraction) of waves



$z=0$ plane

θ_I = angle of incidence
θ_R = angle of reflection
θ_T = angle of transmission (refraction)

wave traveling from a to b.

assume $\begin{cases} \mu_a \text{ and } \mu_b \text{ are real} \\ \varepsilon_a \text{ real} \\ \varepsilon_b \text{ may be complex} \end{cases}$

$$\vec{E}_I = \vec{E}_{\omega I}\, e^{i(\vec{k}_I\cdot\vec{r}-\omega_I t)}$$

$$\vec{E}_R = \vec{E}_{\omega R}\, e^{i(\vec{k}_R\cdot\vec{r}-\omega_R t)}$$

$$\vec{E}_T = \vec{E}_{\omega T}\, e^{i(\vec{k}_T\cdot\vec{r}-\omega_T t)}$$

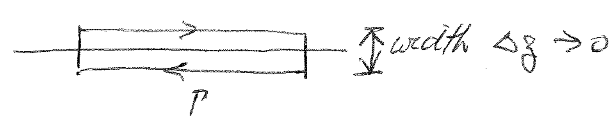
similarly for $\vec{H}_I$, $\vec{H}_R$, $\vec{H}_T$

in each media $k^2 = \frac{\omega^2}{c^2}\frac{\mu}{\mu_0}\frac{\varepsilon}{\varepsilon_0} = \omega^2\mu\varepsilon$

$$k_I^2 = \omega_I^2\mu_a\varepsilon_a\ ,\quad k_R^2 = \omega_R^2\mu_a\varepsilon_a\ ,\quad k_T^2 = \omega_T^2\mu_b\varepsilon_b$$

boundary conditions at interface

Faraday $\quad \vec{\nabla}\times\vec{E}_\omega - i\omega\mu\vec{H}_\omega = 0$



$$\int_S d\vec{a}\cdot(\vec{\nabla}\times\vec{E}_\omega) = \int_S d\vec{a}\cdot\vec{H}_\omega\, i\omega\mu \to 0 \text{ as } \Delta z\to 0$$

surface bounded by Γ

$$\oint_\Gamma d\vec{l}\cdot\vec{E}_\omega \Rightarrow (\vec{E}_{above}-\vec{E}_{below})\cdot d\vec{l} = 0$$

$\Rightarrow$ tangential component of $\vec{E}$ is continuous as cross interface

Ampere $\nabla \times \vec{H}_\omega = -i\omega\varepsilon \vec{E}_\omega$ (assuming no free current at boundary)

same argument as for $\vec{E}$ $\Rightarrow$ tangential component of $\vec{H}$ is continuous at interface

apply to $\vec{E}$ at interface: For $\hat{t}$ any unit vector in xy plane

$$\hat{t}\cdot(\vec{E}_I + \vec{E}_R) = \hat{t}\cdot\vec{E}_T$$

$\Rightarrow$ for any $\vec{\rho}$ in xy plane at $z=0$, and any time t

$$\hat{t}\cdot\vec{E}_{\omega I}\, e^{i(\vec{k}_I\cdot\vec{\rho} - \omega_I t)} + \hat{t}\cdot\vec{E}_{\omega R}\, e^{i(\vec{k}_R\cdot\vec{\rho} - \omega_R t)}$$

$$= \hat{t}\cdot\vec{E}_{\omega T}\, e^{i(\vec{k}_T\cdot\vec{\rho} - \omega_T t)}$$

true for any $\vec{\rho}$, so consider at $\vec{\rho}=0$

$$\hat{t}\cdot\vec{E}_{\omega I}\, e^{-i\omega_I t} + \hat{t}\cdot\vec{E}_{\omega R}\, e^{-i\omega_R t} = \hat{t}\cdot\vec{E}_{\omega T}\, e^{-i\omega_T t}$$

must be true for all t $\Rightarrow$ $\boxed{\omega_I = \omega_R = \omega_T}$
all freq's equal

Now consider for $\rho \neq 0$, at $t=0$.

$$\hat{t}\cdot\vec{E}_{\omega I}\, e^{i\vec{k}_I\cdot\vec{\rho}} + \hat{t}\cdot\vec{E}_{\omega R}\, e^{i\vec{k}_R\cdot\vec{\rho}} = \hat{t}\cdot\vec{E}_{\omega T}\, e^{i\vec{k}_T\cdot\vec{\rho}}$$

must be true for all $\vec{\rho}$ $\Rightarrow$ $\vec{k}_I \cdot \vec{\rho} = \vec{k}_R \cdot \vec{\rho} = \vec{k}_T \cdot \vec{\rho}$ all ρ

$\Rightarrow$ projections of $\vec{k}_I, \vec{k}_R, \vec{k}_T$ in xy plane are all equal.
only z-components of $\vec{k}_I, \vec{k}_R, \vec{k}_T$ may differ

Choose coordinates as in diagram so that all $\vec{k}$'s lie in xz plane.

$$k_{Ix} = k_{Rx} \Rightarrow |\vec{k}_I| \sin\theta_I = |\vec{k}_R| \sin\theta_R$$

$$|\vec{k}_I| = \omega\sqrt{\mu_a \varepsilon_a} = |\vec{k}_R| \Rightarrow \boxed{\theta_I = \theta_R}$$

<u>angle of incidence = angle of reflection</u>

If $\sqrt{\varepsilon_b}$ is also real (ie in region of transparent propagation)

then $|\vec{k}_T| = \omega\sqrt{\mu_b \varepsilon_b}$

$$k_{Ix} = k_{Tx} \Rightarrow |\vec{k}_I| \sin\theta_I = |\vec{k}_T| \sin\theta_T$$

$$\omega\sqrt{\mu_a \varepsilon_a} \sin\theta_I = \omega\sqrt{\mu_b \varepsilon_b} \sin\theta_T$$

$$\frac{\sin\theta_T}{\sin\theta_I} = \sqrt{\frac{\mu_a \varepsilon_a}{\mu_b \varepsilon_b}}$$

in terms of index of refraction $n \equiv \frac{kc}{\omega} = \frac{\omega\sqrt{\mu\varepsilon}\, c}{\omega}$

$n \equiv \frac{c}{v_p}$ $\qquad = \sqrt{\mu\varepsilon}\, c = \sqrt{\frac{\mu\varepsilon}{\mu_0\varepsilon_0}}$

$$\boxed{\frac{\sin\theta_T}{\sin\theta_I} = \frac{n_a}{n_b}}$$

<u>Snell's law</u> – true for all types of waves, not just EM waves

$$\sin\theta_T = \frac{n_a}{n_b}\sin\theta_I$$

If $n_a > n_b$, then $\theta_T > \theta_I$

in this case,

when θ_I is too large, we will have $\frac{n_a}{n_b}\sin\theta_I > 1$

and there is no solution for θ_T

$\Rightarrow \vec{E}_T = 0$, there is no transmitted wave.

this is called "total internal reflection" – wave does not exit medium a.

critical angle $\theta_c = \arcsin\left(\frac{n_b}{n_a}\right)$ ← the bigger n_a/n_b, the smaller θ_c

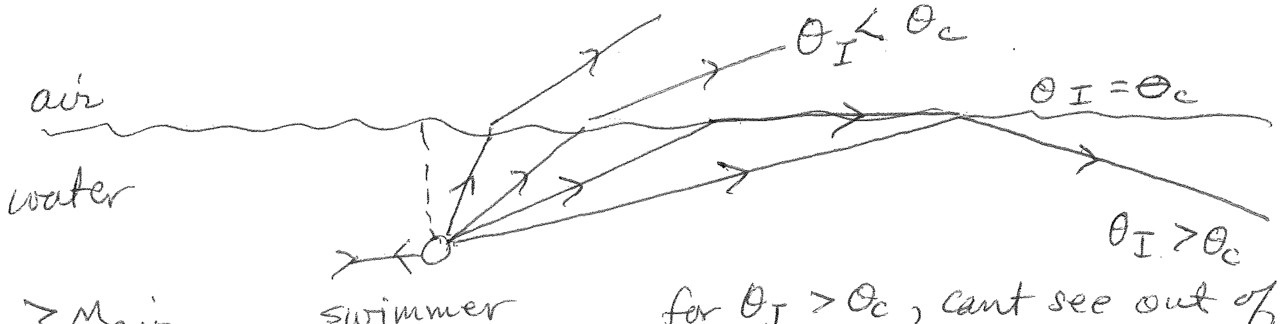
total internal reflection whenever $\theta_I > \theta_c$

total internal reflection usually happens as one goes from a <u>denser</u> to a <u>less dense</u> ~~mater~~ medium as

$\mu\epsilon \sim \mu\epsilon_0\left(1 + \frac{Ne^2}{m\epsilon_0}\right)$ where N is density of polarizable atoms (m is electron mass).

total internal reflection is why diamonds sparkle! diamond has big n ⇒ small θ_c ⇒ light bounces around inside diamond getting totally internally reflected many times, before it is able to escape.

Can also experience total internal reflection in the swimming pool:

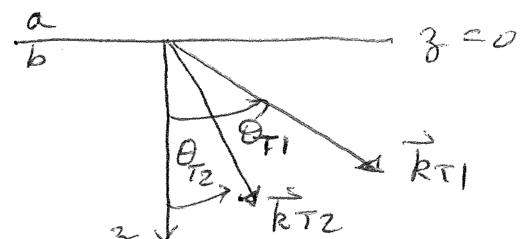


$n_{water} > n_{air}$

for $\theta_I > \theta_c$, can't see out of water

when $\theta_I = \theta_c$, transmitted wave travels parallel to interface

<u>More general case</u>: $\sqrt{\varepsilon_b}$ can be complex $\Rightarrow \vec{k}_T$ is complex



$$\vec{k}_T = \vec{k}_{T1} + i\vec{k}_{T2}$$

$$k_{T1} \equiv |\vec{k}_{T1}| \quad , \quad k_{T2} \equiv |\vec{k}_{T2}|$$

$\vec{k}_{T1}$ and $\vec{k}_{T2}$ need not be in same direction!

$$\vec{k}_{Tx} = \vec{k}_{Ix} \Rightarrow k_{T1}\sin\theta_{T1} + i k_{T2}\sin\theta_{T2} = k_I \sin\theta_I$$

equate real and imaginary pieces $\Rightarrow$ $\boxed{\begin{array}{l} k_{T1}\sin\theta_{T1} = k_I \sin\theta_I \\ k_{T2}\sin\theta_{T2} = 0 \end{array}}$

$\Rightarrow \boxed{\theta_{T2} = 0}$

ie attenuation factor for the transmitted wave is of the form $e^{-k_{T2} z}$

$\Rightarrow$ planes of constant <u>amplitude</u> are <u>parallel</u> to the interface, no matter what the angle of incidence θ_I.