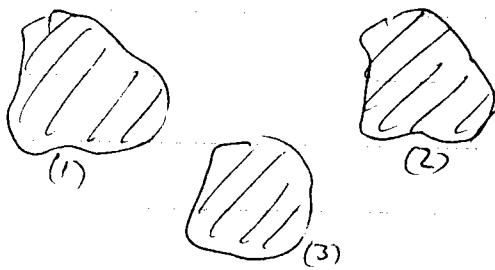


Capacitance

Consider a set of conductors with potential $\phi(\vec{r}) = V_i$ fixed on conductor i



(also need condition on
 $V(\vec{r}) \rightarrow \infty$ if system is
 not enclosed)

From uniqueness theorem we know that specifying the V_i on each conductor is enough to determine the potential $\phi(\vec{r})$ everywhere. We can write this potential in the following form -

Let $\phi^{(i)}(\vec{r})$ be the solution to the boundary value problem
 $\nabla^2 \phi^{(i)}(\vec{r}) = 0$ and $\phi^{(i)}(\vec{r}) = \begin{cases} 1 & \text{if } \vec{r} \text{ on surface of conductor } i \\ 0 & \text{if } \vec{r} \text{ on surface of any other conductor } j, j \neq i \end{cases}$

Then by superposition

$$\phi(\vec{r}) = \sum_i V_i \phi^{(i)}(\vec{r})$$

is solution to the problem $\nabla^2 \phi = 0$ and $\phi(\vec{r}) = V_i$ for \vec{r} on surface of conductor (i)

The surface charge density at \vec{r} on surface of conductor (i) is

$$\sigma^{(i)}(\vec{r}) = \frac{-1}{4\pi} \frac{\partial \phi(\vec{r})}{\partial \vec{n}} = -\frac{1}{4\pi} \sum_j V_j \frac{\partial \phi^{(j)}(\vec{r})}{\partial \vec{n}}$$

Where $\frac{\partial \phi}{\partial \vec{n}} = (\vec{\nabla} \phi) \cdot \hat{\vec{n}}$ is the derivative normal to the surface at point \vec{r} .

The total charge on conductor (i) is

$$Q_i = \int_{S_i} da \sigma^{(i)}(\vec{r}) = -\frac{1}{4\pi} \sum_j V_j \int_{S_i} da \frac{\partial \phi^{(j)}}{\partial n}$$

↑
surface of conductor(i)

Define $C_{ij} = -\frac{1}{4\pi} \int_{S_i} da \frac{\partial \phi^{(j)}}{\partial n}$

the C_{ij} depend only on
the geometry of the
conductors

Then we have

$$Q_i = \sum_j C_{ij} V_j$$

C_{ij} is the capacitance matrix

The charge on conductor (i) is a linear function of the potentials V_j on the conductors (j)

Since we know that specifying the Q_i that is on each conductor will uniquely determine $\phi(\vec{r})$ and hence the potential V_i on each conductor, the capacitance matrix is invertable

$$V_i = \sum_j [C^{-1}]_{ij} Q_j$$

The electrostatic energy of the conductors is then

$$\mathcal{E} = \frac{1}{2} \int d^3r \rho \phi = \frac{1}{2} \sum_i Q_i V_i = \frac{1}{2} \sum_{i,j} C_{ij} V_i V_j$$

Convene to define Capacitance of two conductors by

$$C = \frac{Q}{V_1 - V_2}$$

when conductor(1) has charge Q
conductor(2) has charge $-Q$

$V_1 - V_2$ is potential difference
between the two conductors.

all other conductors fixed at $V_i = 0$

We can determine C in terms of the elements of the matrix C_{ij}

$$\begin{aligned} Q &= C_{11}V_1 + C_{12}V_2 \\ -Q &= C_{21}V_1 + C_{22}V_2 \end{aligned} \quad \Rightarrow \quad V_2 = -\left(\frac{C_{11} + C_{21}}{C_{12} + C_{22}}\right)V_1$$

$$\Rightarrow Q = \left[C_{11} - C_{12} \left(\frac{C_{11} + C_{21}}{C_{12} + C_{22}} \right) \right] V_1$$

$$V_1 - V_2 = \left[1 + \left(\frac{C_{11} + C_{21}}{C_{12} + C_{22}} \right) \right] V_1$$

$$C = \frac{Q}{V_1 - V_2} = \frac{C_{11} - C_{12} \left(\frac{C_{11} + C_{21}}{C_{12} + C_{22}} \right)}{1 + \left(\frac{C_{11} + C_{21}}{C_{12} + C_{22}} \right)}$$

$$C = \frac{C_{11}C_{22} - C_{12}C_{21}}{C_{11} + C_{12} + C_{21} + C_{22}}$$

Capacitance can also be defined when the space between the conductors is filled with a dielectric ϵ

In this case, if Q_i is the free charge, then Q_i/ϵ is the effective total charge to use in computing ϕ .

$$\Rightarrow \frac{Q_i}{\epsilon} = \sum_j C_{ij}^{(0)} V_j \quad \text{where } C_{ij}^{(0)} \text{ are capacitances appropriate to a vacuum between the conductors}$$

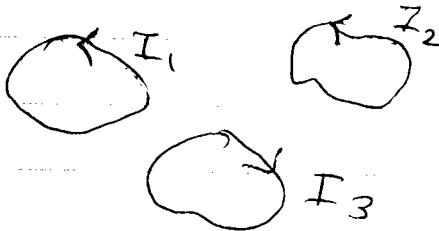
$$\Rightarrow Q_i = \sum_j \epsilon C_{ij}^{(0)} V_j$$

$$= \sum_j C_{ij} V_j \quad \text{where } C_{ij} = \epsilon C_{ij}^{(0)}$$

the capacitance is increased by a factor the dielectric constant ϵ .

Inductance

Consider a set of current carrying loops C_i with currents I_i .



In Coulomb gauge, we can write the magnetic vector potential \vec{A} from these current loops as

$$\vec{A}(\vec{r}) = \frac{1}{c} \int d^3 r' \frac{\vec{j}(\vec{r}')}{|\vec{r} - \vec{r}'|} = \sum_i \frac{I_i}{c} \oint_{C_i} \frac{d\vec{l}'}{|\vec{r} - \vec{r}'|}$$

↑ integrate over loop C_i
integration variable is \vec{r}'

The magnetic flux through loop i is

$$\Phi_i = \iint_{S_i} da \hat{n} \cdot \vec{B} = \iint_{S_i} da \hat{n} \cdot \vec{\nabla} \times \vec{A} = \oint_{C_i} d\vec{l} \cdot \vec{A}$$

↑ surface bounded
by loop C_i

$$\Phi_i = \sum_j \frac{I_j}{c} \oint_{C_i} \oint_{C_j} \frac{d\vec{l}_i \cdot d\vec{l}_j}{|\vec{r} - \vec{r}'|}$$

↓ pure geometrical quantity

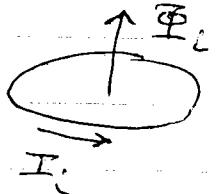
$$\Phi_i = c \sum_j M_{ij} I_j$$

where $M_{ij} = \oint_{C_i} \oint_{C_j} \frac{d\vec{l}_i \cdot d\vec{l}_j}{c^2 |\vec{r} - \vec{r}'|}$

is the mutual inductance of loops (i) and (j). $M_{ij} = M_{ji}$

$L_i \equiv M_{ii}$ is self-inductance of loop (i)

The sign convention in the above is that, Φ_i is computed in direction given by right hand rule, according to the direction taken for current in loop (i)



Magneto static energy

$$\begin{aligned} E &= \frac{1}{2c} \int d^3r \vec{J} \cdot \vec{A} = \frac{1}{2c} \sum_i \oint_{C_i} d\vec{l} \cdot \vec{A} I_i \\ &= \frac{1}{2c} \sum_i \Phi_i I_i \end{aligned}$$

$$E = \frac{1}{2} \sum_{i,j} M_{ij} I_i I_j$$

Force and Torque on electric dipoles

localized charge distribution $\rho(\vec{r})$ with net charge $\int d^3r \rho = 0$

force on ρ in slowly varying electric field \vec{E} is

$$\vec{F} = \int d^3r \rho(\vec{r}) \vec{E}(\vec{r})$$

define $\vec{r} = \vec{r}_0 + \vec{r}'$ where \vec{r}_0 is some fixed reference point
in center of charge distribution ρ , and \vec{r}'
is distance relative to \vec{r}_0

$$\vec{F} = \int d^3r' \rho(\vec{r}') \vec{E}(\vec{r}_0 + \vec{r}')$$

since \vec{E} is slowly varying on length scale where $\rho \neq 0$,
we expand

$$\vec{F} \approx \int d^3r' \rho(\vec{r}') \left[\vec{E}(\vec{r}_0) + (\vec{r}' \cdot \vec{\nabla}) \vec{E}(\vec{r}_0) \right] + \dots$$

$$= \vec{E}(\vec{r}_0) \int d^3r' \rho(\vec{r}') + \left(\int d^3r' \rho(\vec{r}') \vec{r}' \cdot \vec{\nabla} \right) \vec{E}(\vec{r}_0)$$

$$= 0 + (\vec{\rho} \cdot \vec{\nabla}) \vec{E}(\vec{r}_0)$$

$$\boxed{\vec{F} = (\vec{\rho} \cdot \vec{\nabla}) \vec{E} = \sum_{\alpha=1}^3 p_\alpha \frac{\partial \vec{E}}{\partial r_\alpha}}$$

For $\vec{E} = \text{constant}$, $\vec{F} = 0$

Torque on p is ~~interference with other charges~~

$$\vec{N} = \int d^3r \, p(\vec{r}) \vec{r} \times \vec{E}(F) \cong \int d^3r \, p(\vec{r}) \vec{r} \times [\vec{E}(\vec{r}_0) + \dots]$$

to lowest order

$$\boxed{\vec{N} = \vec{p} \times \vec{E}}$$

Force and torque on magnetic dipoles

localized magneto static current distribution $\vec{j}(\vec{r})$

$$\vec{F} = \frac{i}{c} \int d^3r \, \vec{j} \times \vec{B}$$

expand about center of current \vec{r}_0

$$\vec{B}(\vec{r}) \cong \vec{B}(\vec{r}_0) + (\vec{r}' \cdot \vec{\nabla}) \vec{B}(\vec{r}_0) + \dots$$

$$\vec{F} = \frac{i}{c} \left[\int d^3r' \, \vec{j}(\vec{r}') \times \vec{B}(\vec{r}_0) + \frac{i}{c} \int d^3r' \, \vec{j}(\vec{r}') \times (\vec{r}' \cdot \vec{\nabla}) \vec{B}(\vec{r}_0) \right]$$

from discussion of magnetic dipole approx we had $\int d^3r \, \vec{j} = 0$

for magnetostatics where $\vec{\nabla} \cdot \vec{j} = 0$, so 1st term vanishes,

The 2nd term can be written as

$$\vec{F}_d = \frac{\epsilon_0 \sigma}{c} \int d^3r' \, \vec{j}_\beta \, r'_s \partial_s B_\gamma \quad \text{for magnetostatics} \\ \text{see magnetic dipole derivation}$$

$$\text{we need the tensor } \frac{1}{c} \int d^3r' \, \vec{j}_\beta \, r'_s = -\frac{1}{c} \int d^3r' \, r'_\beta \, j_s$$

$$= \frac{1}{2c} \int d^3r' \left[\vec{j}_\beta r'_s - r'_\beta \vec{j}_s \right]$$

$$= -M_0 \, \epsilon_0 \, \sigma$$

$$\uparrow \text{magnetic dipole } \vec{m} = \frac{1}{2c} \int d^3r \, \vec{r} \times \vec{j}$$

$$\begin{aligned}
 F_\alpha &= \epsilon_{\alpha\beta\gamma} \epsilon_{\sigma\delta\tau} (-m_\sigma) \partial_\delta B_\gamma \\
 &= -(\delta_{\alpha 0} \delta_{\gamma 0} - \delta_{\alpha 0} \delta_{\sigma 0}) m_\sigma \partial_\gamma B_\sigma \\
 &= \text{M.M. } \vec{\nabla}_\alpha (\vec{m} \cdot \vec{B}) - \vec{m}_\alpha \vec{\nabla} \cdot \vec{B}
 \end{aligned}$$

$$\boxed{\vec{F} = \vec{\nabla} (\vec{m} \cdot \vec{B})} \quad \text{as } \vec{\nabla} \cdot \vec{B} = 0$$

torque on \vec{f} is

$$\begin{aligned}
 \vec{N} &= \frac{1}{c} \int d^3r \vec{r} \times (\vec{f} \times \vec{B}) \quad \text{to lowest order, } \vec{B} = \vec{B}(\vec{r}_0) \\
 &\quad \text{is const over region where } \vec{f} \neq 0 \\
 &= \frac{1}{c} \int d^3r [\vec{f} (\vec{r} \cdot \vec{B}) - \vec{B} (\vec{r} \cdot \vec{f})]
 \end{aligned}$$

2nd term = 0 as follows

$$\begin{aligned}
 \int d^3r \vec{r} \cdot \vec{f} &= \int d^3r \vec{f} \cdot \vec{\nabla} \left(\frac{r^2}{2} \right) \quad \text{as } \vec{\nabla} \left(\frac{r^2}{2} \right) = \vec{r} \\
 &= - \int d^3r (\vec{r} \cdot \vec{f}) \left(\frac{r^2}{2} \right) \quad \text{integrate by parts.} \\
 &\quad \text{Surface term} \rightarrow 0 \text{ as} \\
 &\quad \vec{f} \text{ is localized} \\
 &= 0 \quad \text{as } \vec{\nabla} \cdot \vec{f} = 0 \text{ in magnetostatics}
 \end{aligned}$$

1st term involves

see derivation of
magnetic dipole approx

$$\int d^3r \vec{f} \vec{r} = - \int d^3r \vec{r} \vec{f} = \frac{1}{2} \int d^3r [\vec{f} \vec{r} - \vec{r} \vec{f}]$$

So

$$\vec{N} = \frac{1}{2c} \int d^3r [\vec{f} (\vec{r} \cdot \vec{B}) - \vec{r} (\vec{f} \cdot \vec{B})]$$

$$\vec{N} = \frac{1}{2c} \int d^3r \left[\vec{j}(\vec{r}, \vec{B}) - \vec{r}(\vec{j} \cdot \vec{B}) \right]$$

$\vec{r} \sim \vec{r} \times \vec{B}$

$$= \frac{1}{2c} \int d^3r (\vec{r} \times \vec{j}) \times \vec{B}$$

$$\boxed{\vec{N} = \vec{m} \times \vec{B}}$$