

$$\vec{A}(\vec{r}) = \int \frac{d^3r'}{c} \frac{\vec{j}(\vec{r}')}{r} + \int \frac{d^3r'}{c} \vec{j}(\vec{r}') \frac{(\vec{r} \cdot \vec{r}')}{r^3} + \dots$$

Consider term ①

$$\int d^3r \vec{j}(\vec{r}) \quad \int d^3r (\vec{j} \cdot \vec{r}) \vec{r} \quad \frac{\partial r_i}{\partial r_j} = \delta_{ij}$$

write $\int d^3r j_i(r) = \sum_{j=1}^3 \int d^3r j_j \frac{\partial r_i}{\partial r_j}$ integrate by parts

$$= \sum_j \left\{ \oint_S da j_j r_i - \int d^3r \frac{\partial j_j}{\partial r_j} r_i \right\}$$

↑
vanishes as $S \rightarrow \infty$ if
 $\vec{j}$ sufficiently localized
ie $\vec{j}(\vec{r}) \rightarrow 0$ sufficiently
fast as $r \rightarrow \infty$

↑
vanishes in
magnetostatics
where $\vec{\nabla} \cdot \vec{j} = 0$

So $\int d^3r \vec{j}(\vec{r}) = 0$ in magnetostatics
monopole term vanishes

term (2)

$$\int d^3r \vec{f}(\vec{r}) \vec{r} \quad \text{tensor}$$

$$\text{Consider } \int d^3r j_i r_j = \sum_k \int d^3r j_k r_j \frac{\partial r_i}{\partial r_k} \quad \text{integrate by parts}$$

$$= \sum_k \left\{ \oint_S da j_k r_j r_i - \int d^3r \frac{\partial}{\partial r_k} (j_k r_j) r_i \right\}$$

$\uparrow$
vanishes as $S \rightarrow \infty$ if $\vec{j}$ sufficiently localized

$$= - \sum_k \int d^3r \left(\frac{\partial j_k}{\partial r_k} r_j r_i + j_k \frac{\partial r_j}{\partial r_k} r_i \right)$$

$\uparrow$ vanishes as $\vec{\nabla} \cdot \vec{j} = 0$ in magnetostatics $\uparrow = \delta_{jk}$

$$= - \int d^3r j_j r_i$$

$$\text{So } \int d^3r j_i r_j = - \int d^3r j_j r_i$$

$$= \frac{1}{2} \int d^3r (j_i r_j - j_j r_i)$$

So

$$\int d^3r' j_i(\vec{r}') (\vec{r} \cdot \vec{r}') = \sum_j r_j \int d^3r' j_i(\vec{r}') r_j'$$

$$= \sum_j \frac{1}{2} \int d^3r' (j_i r_j r_j' - r_j j_j r_i')$$

$$= \frac{1}{2} \int d^3r' (j_i (\vec{r} \cdot \vec{r}') - r_i' (\vec{r} \cdot \vec{r}'))$$

use triple product rule

$$\vec{r} \times (\vec{r}' \times \vec{f}) = \vec{r}' (\vec{r} \cdot \vec{f}) - \vec{f} (\vec{r} \cdot \vec{r}')$$

to rewrite as

$$\int d^3r' \vec{f} (\vec{r} \cdot \vec{r}') = -\frac{1}{2} \vec{r} \times \left[\int d^3r' \vec{r}' \times \vec{f} (\vec{r}') \right]$$

define the magnetic dipole moment as

$$\boxed{\vec{m} \equiv \frac{1}{2c} \int d^3r' \vec{r}' \times \vec{f} (\vec{r}')}$$

In magnetic dipole approx (this is the lowest non-vanishing term)

$$\vec{A}(\vec{r}) = -\frac{\vec{r} \times \vec{m}}{r^3} = \frac{\vec{m} \times \vec{r}}{r^3} = \frac{\vec{m} \times \hat{r}}{r^2}$$

$$\vec{B} = \vec{\nabla} \times \vec{A} = \vec{\nabla} \times \left(\frac{\vec{m} \times \vec{r}}{r^3} \right)$$

$$B_i = \epsilon_{ijk} \partial_j \epsilon_{klm} m_l \frac{r_m}{r^3}$$

$$= (\delta_{il} \delta_{jm} - \delta_{im} \delta_{jl}) \partial_j m_l \frac{r_m}{r^3}$$

$$= m_i \partial_j \left(\frac{r_j}{r^3} \right) - m_j \partial_j \left(\frac{r_i}{r^3} \right)$$

$$= m_i \left[-4\pi \delta(\vec{r}) \right] - m_j \left[\frac{\delta_{ij}}{r^3} - \frac{3r_i}{r^4} \partial_j r \right]$$

$$= \underset{\text{for beam source}}{0} - \frac{m_i}{r^3} + \frac{3r_i}{r^4} \frac{r_j m_j}{r}$$

Levi-Civita symbol

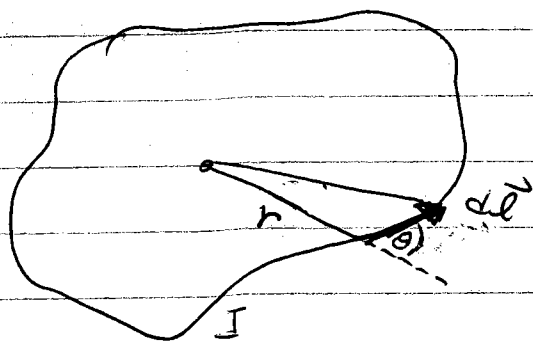
$$\epsilon_{ijk} = \begin{cases} 0, & \text{any two indices equal} \\ +1, & \text{ijk even permute of 123} \\ -1, & \text{ijk odd permute of 123} \end{cases}$$

$$\vec{B} = \frac{3(\vec{m} \cdot \hat{r})\hat{r} - \vec{m}}{r^3}$$

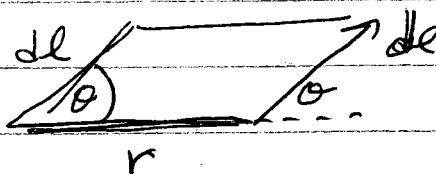
same form as $\vec{E}$ from electric dipole $\vec{p}$

For a current loop in a plane (any shape loop provided it is flat)

$$\vec{m} = \frac{1}{2c} \int d^3r \vec{r} \times \vec{j} = \frac{1}{2c} I \oint \vec{r} \times d\vec{\ell}$$



area of triangle is $\frac{1}{2} r d\ell \sin \theta$
 $= \frac{1}{2} |\vec{r} \times d\vec{\ell}|$



area of rectangle is $r d\ell \sin \theta$

$$\Rightarrow \vec{m} = \frac{1}{2} I (\text{area}) \hat{n}$$

↑
area of loop

↖ outward normal

(direction given by right hand rule with respect to direction of current)

magnetic dipole moment $\vec{m}$ is independent of location of origin.

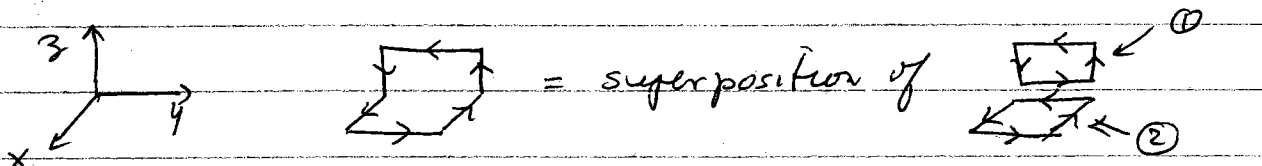
$$\vec{r}' = \vec{r} + \vec{d} \quad \text{new coord}$$

$$\begin{aligned} \vec{m}' &= \frac{1}{2c} \int d^3r' (\vec{r}' \times \vec{j}) = \frac{1}{2c} \int d^3r (\vec{r} + \vec{d}) \times \vec{j} \\ &= \frac{1}{2c} \int d^3r \vec{r} \times \vec{j} + \frac{1}{2c} \vec{d} \times \left[\int d^3r \vec{j} \right] \end{aligned}$$

$$\vec{m}' = \vec{m} + 0 \quad \text{as } \int d^3r \vec{j} = 0$$

for planar loop $\vec{m} = \frac{Ia}{c} \hat{n}$ where $a = \text{area}$
 $\hat{n} = \text{outward normal}$

can also apply to get $\vec{m}$ for piecewise planar loops



$$\begin{aligned} \vec{m} &= \vec{m}_1 + \vec{m}_2 & \vec{m}_1 &= \frac{Ia_1}{c} \hat{x} \\ & & \vec{m}_2 &= \frac{Ia_2}{c} \hat{z} \\ \Rightarrow \vec{m} &= \frac{I}{c} (a_1 \hat{x} + a_2 \hat{z}) \end{aligned}$$

Boundary value problems in magnetostatics

Scalar Magnetic Potential

Because of the vector character of the equation

$$-\nabla^2 \vec{A} = \frac{4\pi}{c} \vec{j}$$

and the fact that $\nabla^2 \vec{A}$ only has a convenient representation in Cartesian coordinates, many of the methods we used to solve the scalar $-\nabla^2 \phi = 4\pi\rho$ don't work so well for magnetostatics.

However, in situations where the current $\vec{j}$ is confined to certain surfaces, we can make things much closer to the electrostatic case by using the trick of the scalar magnetic potential ϕ_M .

In regions where $\vec{j} = 0$, i.e. not on the certain surfaces, we have $\vec{\nabla} \cdot \vec{B} = 0$ and $\vec{\nabla} \times \vec{B} = 0$. Since $\vec{\nabla} \times \vec{B} = 0$ in these regions we can define a scalar potential ϕ_M such that

$$\vec{B} = -\vec{\nabla} \phi_M$$

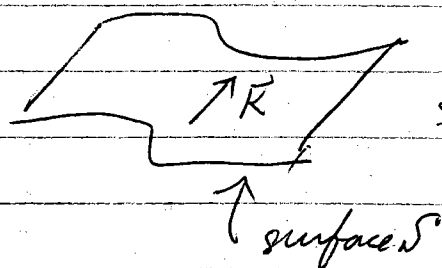
and then

$$\vec{\nabla} \cdot \vec{B} = -\nabla^2 \phi_M = 0$$

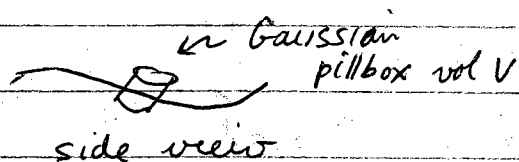
We can solve for ϕ_M as in electrostatics, and match solutions by applying appropriate boundary conditions on the current carrying surfaces.

Boundary Conditions at sheet current

in magnetostatics $\vec{\nabla} \cdot \vec{B} = 0$, $\vec{\nabla} \times \vec{B} = \frac{4\pi}{c} \vec{j}$



surface current $\vec{K}(\vec{r})$ at pt $\vec{r}$
on surface S



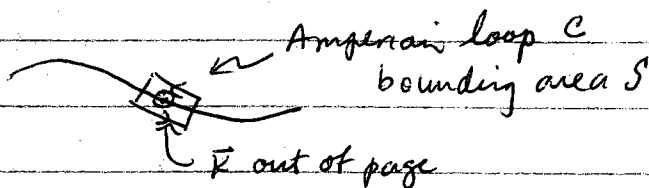
side view

$$\int_V d^3r \vec{\nabla} \cdot \vec{B} = 0$$

top + bottom area of pill box is da
width of pill box $\rightarrow 0$

$$\Rightarrow \int_V d^3r \vec{\nabla} \cdot \vec{B} = \oint_S da \hat{n} \cdot \vec{B} = da (\vec{B}_{above} - \vec{B}_{below}) \cdot \hat{n} = 0$$

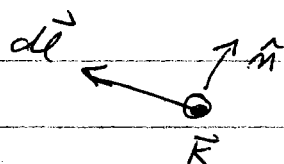
normal component of $\vec{B}$ is continuous $(\vec{B}_{above} - \vec{B}_{below}) \cdot \hat{n} = 0$



side view

$$\int_S da \hat{n} \cdot (\vec{\nabla} \times \vec{B}) = \oint_C \vec{B} \cdot d\vec{l} = \frac{4\pi}{c} I_{enclosed}$$

let width of loop $\rightarrow 0$, top + bottom sides $d\vec{l}$



$$(\hat{n} \times d\vec{l}) = \vec{K}$$

$$(\vec{B}_{above} - \vec{B}_{below}) \cdot d\vec{l} = \frac{4\pi}{c} \vec{K} \cdot \hat{n}$$

$$= \frac{4\pi}{c} (\vec{K} \times \hat{n}) \cdot d\vec{l}$$

$\hat{n}$ is outward
normal

tangential component of $\vec{B}$ has
discontinuous jump $\frac{4\pi}{c} \vec{K} \times \hat{n}$

Combine both results into

$$\vec{B}_{\text{above}} - \vec{B}_{\text{below}} = \frac{4\pi}{c} \vec{K} \times \hat{n}$$

magnetic analog of $\vec{E}_{\text{above}} - \vec{E}_{\text{below}} = 4\pi\sigma \hat{n}$

In terms of magnetic vector potential Φ_M

$$-\vec{\nabla}\Phi_{M\text{above}} + \vec{\nabla}\Phi_{M\text{below}} = \frac{4\pi}{c} \vec{K} \times \hat{n}$$

Note: Φ_M is a calculational tool only
it does not have any direct physical
significance as does the electrostatic ϕ .
Electrostatic ϕ is related to work done
moving a charge $W_{12} = q[\phi(r_2) - \phi(r_1)]$
nothing similar for Φ_M .

(in fact ~~magnetostatic~~ magnetic forces do no work!

$$\vec{F} = q \vec{v} \times \vec{B}$$

$$\Rightarrow \vec{F} \cdot \vec{v} = \frac{dW}{dt} = 0)$$

Note: we cannot apply argument ^{like} $\phi(r) - \phi(r') = \int \vec{E} \cdot d\vec{l}$
 Φ_M is not necessarily continuous at surface "current"
Cannot do similar to electrostatics and use

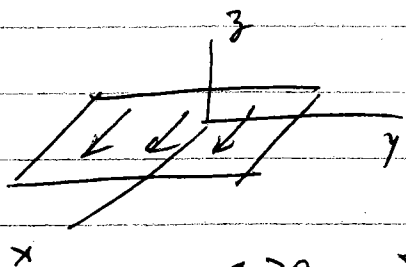
$$\Phi_M(r_{\text{above}}) - \Phi_M(r_{\text{below}}) = - \int_{r_{\text{below}}}^{r_{\text{above}}} \vec{B} \cdot d\vec{l}$$

Since Φ_M is not defined on the current sheet
itself, separating "above" from "below".

example

Flat infinite plane at $z=0$ with surface current

$$\vec{K} = K \hat{x}$$



$$z > 0, \nabla^2 \phi_M^> = 0 \Rightarrow \phi_M^> = a^> - b_x^> x - b_y^> y - b_z^> z$$

$$z < 0, \nabla^2 \phi_M^< = 0 \Rightarrow \phi_M^< = a^< - b_x^< x - b_y^< y - b_z^< z$$

$$z > 0, \vec{B}^> = -\vec{\nabla} \phi_M^> = b_x^> \hat{x} + b_y^> \hat{y} + b_z^> \hat{z}$$

$$z < 0, \vec{B}^< = -\vec{\nabla} \phi_M^< = b_x^< \hat{x} + b_y^< \hat{y} + b_z^< \hat{z}$$

$$\begin{aligned} \text{at } z=0 \quad \vec{B}^> - \vec{B}^< &= (b_x^> - b_x^<) \hat{x} + (b_y^> - b_y^<) \hat{y} + (b_z^> - b_z^<) \hat{z} \\ &= \frac{4\pi}{c} \vec{K} \times \hat{n} = \frac{4\pi}{c} K (\hat{x} \times \hat{z}) = -\frac{4\pi K}{c} \hat{y} \end{aligned}$$

$$\Rightarrow b_x^> = b_x^< \equiv b_{x0}, \quad b_z^> = b_z^< \equiv b_{z0}, \quad b_y^> - b_y^< = -\frac{4\pi K}{c}$$

$$\begin{aligned} \text{define } \left. \begin{aligned} b_y^> &= b_{y0} + \delta b_y \\ b_y^< &= b_{y0} - \delta b_y \end{aligned} \right\} \delta b_y &= -\frac{2\pi K}{c} \end{aligned}$$

$$\begin{aligned} \Rightarrow \vec{B}^> &= \vec{B}_0 - \frac{2\pi K}{c} \hat{y} & \vec{B}_0 &= b_{x0} \hat{x} + b_{y0} \hat{y} + b_{z0} \hat{z} \\ \vec{B}^< &= \vec{B}_0 + \frac{2\pi K}{c} \hat{y} \end{aligned}$$

if $\vec{K}$ is the only source of magnetic field then $\vec{B}_0 = 0$

$$\vec{B} = \begin{cases} -\frac{2\pi K}{c} \hat{y} & z > 0 \\ \frac{2\pi K}{c} \hat{y} & z < 0 \end{cases}$$