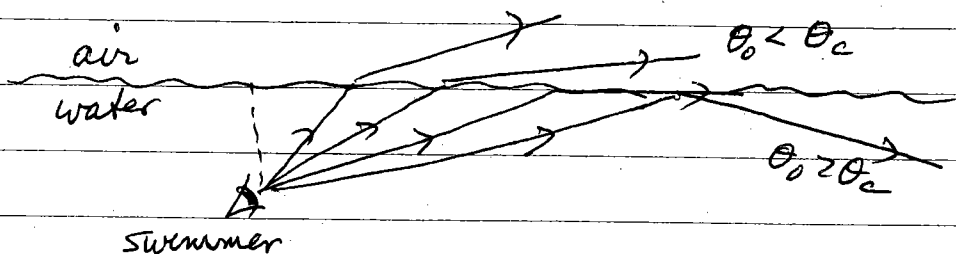


$$\epsilon \sim 1 + 4\pi N \alpha \quad \leftarrow \text{density}$$

Since $n \propto \sqrt{\mu\epsilon}$ and ϵ grows with density of the material, one usually has total internal reflection when one goes from a denser to a less dense medium.

Examples: diamonds sparkle due to total internal reflection. Diamonds have large $n \Rightarrow$ small $\theta_c \Rightarrow$ light bounces around inside many times before it can exit.

Can also see total internal reflection when swimming under water.



More general case $\sqrt{\epsilon_2}$ is complex so $\vec{k}_2$ is complex

$$\vec{k}_2 = \vec{k}_2' + i\vec{k}_2''$$

$$k_2' = |\vec{k}_2'|$$

$$k_2'' = |\vec{k}_2''|$$

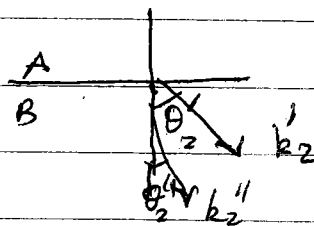
↑ ↑
real part imaginary part

Note $\vec{k}_2'$ and $\vec{k}_2''$ need not be in the same direction!

Condition $k_{0x} = k_{2x} \Rightarrow \begin{cases} k_{0x} = k_{2x}' \\ 0 = k_{2x}'' \end{cases}$ equate real and imaginary parts

$$k_0 \sin \theta_0 = k_2' \sin \theta_2'$$

$$0 = k_2'' \sin \theta_2''$$



$\Rightarrow \theta_2'' = 0$
 $\vec{k}_2'' = k_2'' \hat{z}$

{ attenuation factor for the transmitted wave is $e^{-k_2'' z}$

$\rightarrow$ planes of constant amplitude are parallel to the interface no matter what the angle of incidence θ_0 .

$k_0 \sin \theta_0 = k_2' \sin \theta_2'$ $\leftarrow$ need two equations to solve for k_2' and θ_2'

$k_0 = \frac{\omega}{c} \sqrt{\mu_a \epsilon_a} = \frac{\omega}{c} n_a$

The 2nd equation comes from dispersion relation in medium (b)

planes of constant phase are $\perp$ to $\vec{k}_2'$

$\vec{k}_2^2 = \vec{k}_2' \cdot \vec{k}_2' = (k_2')^2 - (k_2'')^2 + 2i \vec{k}_2' \cdot \vec{k}_2'' = \frac{\omega^2}{c^2} \mu_b \epsilon_b$

dispersion relation

$\vec{k}_2' \cdot \vec{k}_2'' = k_2' k_2'' \cos \theta_2'$

equate real and imaginary parts

$(k_2')^2 - (k_2'')^2 = \frac{\omega^2}{c^2} \mu_b \epsilon_{b1}$

$2 k_2' k_2'' \cos \theta_2' = \frac{\omega^2}{c^2} \mu_b \epsilon_{b2}$

$\epsilon_b = \epsilon_{b1} + i \epsilon_{b2}$

$\uparrow \quad \uparrow$
 real

Solve

$(k_2')^2 = (k_2'')^2 + \frac{\omega^2}{c^2} \mu_b \epsilon_{b1}$

$(k_2')^2 = \left(\frac{\omega^2}{c^2} \frac{\mu_b \epsilon_{b2}}{2 k_2' \cos \theta_2'} \right)^2 + \frac{\omega^2}{c^2} \mu_b \epsilon_{b1}$

$$(k_2')^4 - \frac{\omega^2}{c^2} \mu_b \epsilon_{b1} (k_2')^2 - \frac{\omega^4}{c^4} \frac{\mu_b^2 \epsilon_{b2}^2}{4 \cos^2 \theta_2'} = 0$$

quadratic formula

$$(k_2')^2 = \frac{\omega^2 \mu_b \epsilon_{b1}}{c^2} + \sqrt{\frac{\omega^4 \mu_b^2 \epsilon_{b1}^2}{c^4} + \frac{\omega^4 \mu_b^2 \epsilon_{b2}^2}{c^4 4 \cos^2 \theta_2'}}$$

$$k_2' = \frac{\omega}{c} \sqrt{\mu_b} \left[\frac{1}{2} \epsilon_{b1} + \frac{1}{2} \sqrt{\epsilon_{b1}^2 + \frac{\epsilon_{b2}^2}{\cos^2 \theta_2'}} \right]^{1/2}$$

and

$$(k_2'')^2 = (k_2')^2 - \frac{\omega^2}{c^2} \mu_b \epsilon_{b1}$$

$$k_2'' = \frac{\omega}{c} \sqrt{\mu_b} \left[-\frac{1}{2} \epsilon_{b1} + \frac{1}{2} \sqrt{\epsilon_{b1}^2 + \frac{\epsilon_{b2}^2}{\cos^2 \theta_2'}} \right]^{1/2}$$

Note, these reduce to what we had earlier for a plane wave, if we take $\theta_2' = 0$

Both k_2' and k_2'' depend on angle of refraction θ_2'

Finally: $k_2' \sin \theta_2' = \frac{\omega}{c} n_a \sin \theta_0$

$$\Rightarrow n_a \sin \theta_0 = \sqrt{\mu_b \epsilon_{b1}} \left[\frac{1}{2} + \frac{1}{2} \sqrt{1 + \frac{\epsilon_{b2}^2}{\epsilon_{b1}^2 \cos^2 \theta_2'}} \right]^{1/2} \sin \theta_2'$$

determines θ_2' in terms of given θ_0

Cases

① for a nearly transparent material with $\epsilon_{b2} \ll \epsilon_{b1}$

define $n_b = \sqrt{\mu_b \epsilon_{b1}}$ index of refraction

$$m_a \sin \theta_0 = m_b \sin \theta_2' \left[1 + \frac{\epsilon_{b2}^2}{4 \epsilon_{b1}^2 \cos^2 \theta_2'} \right]^{1/2}$$

$$\approx m_b \sin \theta_2' \left[1 + \frac{\epsilon_{b2}^2}{8 \epsilon_{b1}^2 \cos^2 \theta_2'} \right]$$

↑
small correction to
Snell's law

for $\frac{\epsilon_{b2}}{\epsilon_{b1}} \ll 1$ can solve iteratively

to lowest order: $m_a \sin \theta_0 \approx m_b \sin \theta_2'$

$$\Rightarrow \cos^2 \theta_2' = 1 - \sin^2 \theta_2' = 1 - \left(\frac{m_a \sin \theta_0}{m_b} \right)^2$$

so to next order

$$m_a \sin \theta_0 \approx m_b \sin \theta_2' \left[1 + \frac{\epsilon_{b2}^2}{8 \epsilon_{b1}^2 \left(1 - \frac{m_a^2}{m_b^2} \sin^2 \theta_0 \right)} \right]$$

$$\text{or } \sin \theta_2' \approx \frac{m_a \sin \theta_0}{m_b} \frac{1}{\left[1 + \frac{\epsilon_{b2}^2}{8 \epsilon_{b1}^2 \left(1 - \frac{m_a^2}{m_b^2} \sin^2 \theta_0 \right)} \right]}$$

$$\leq \frac{m_a \sin \theta_0}{m_b}$$

result is that θ_2' is smaller than Snell's law would predict.

② for a good conductor, or absorbing region of a dielectric, $\epsilon_{b2} \gg \epsilon_{b1}$

to lowest order

$$n_a \sin \theta_0 = \sqrt{\mu_b \epsilon_{b1}} \left[\frac{1}{2} \frac{\epsilon_{b2}}{\epsilon_{b1} \cos \theta_2'} \right]^{1/2} \sin \theta_2'$$

$$n_a \sin \theta_0 = \sqrt{\frac{\mu_b \epsilon_{b2}}{2}} \frac{\sin \theta_2'}{\sqrt{\cos \theta_2'}}$$

← very different from Snell's Law!

Snell's law only holds if both media are transparent

Reflection coefficients

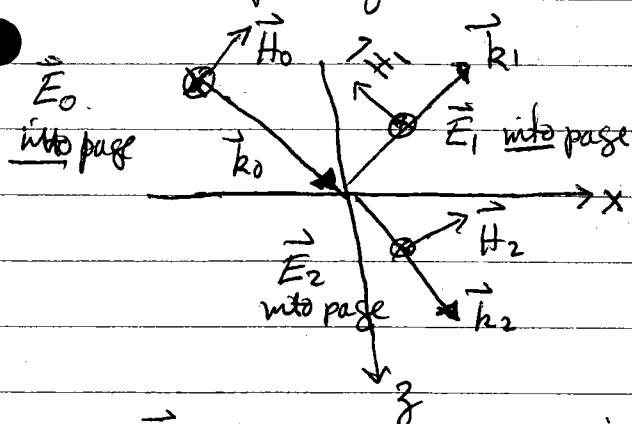
Now we compute the amplitude of the reflected wave to determine how much of incident wave is reflected and how much is transmitted.

Consider two cases ① $\vec{E}_0$ is $\perp$ plane of incidence

② $\vec{E}_0$ lies in the plane of incidence

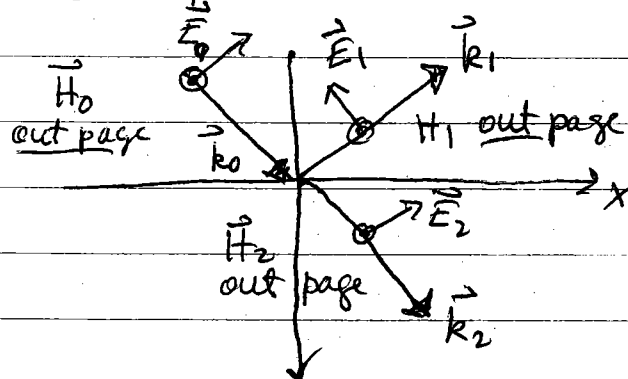
"plane of incidence" is the plane spanned by the wave vector $\vec{k}_0$ and the normal to the interface - in our case it is the xz plane

① $\vec{E}_0 \perp$ plane of incidence



$\Rightarrow \vec{H}_0$ in plane of incidence
all $\vec{E}$'s are in $\hat{y}$ direction

② $\vec{E}_0 \parallel$ plane of incidence



$\Rightarrow \vec{H}_0 \perp$ plane of incidence
all the $\vec{H}$'s are in $\hat{y}$ direction

continuity of y components

$$1) E_0 + E_1 = E_2$$

$$1) H_0 + H_1 = H_2$$

continuity of x components

$$H_{0x} + H_{1x} = H_{2x}$$

$$E_{0x} + E_{1x} = E_{2x}$$

Faraday
 $\frac{c\mu_0}{c} \vec{H} = \vec{\nabla} \times \vec{E} \Rightarrow H_x = \frac{k_z c}{\omega \mu} E_y$

Ampere
 $-\frac{c\omega \epsilon}{c} \vec{E} = \vec{\nabla} \times \vec{H} \Rightarrow E_x = -\frac{k_z c}{\omega \epsilon} H_y$

$$2) \frac{k_{0z}}{\mu_a} (E_0 - E_1) = \frac{k_{2z}}{\mu_b} E_2$$

solve (1) and (2) for
 E_1 and E_2 in terms of E_0

$$E_1 = \frac{\mu_b k_{0z} - \mu_a k_{2z}}{\mu_b k_{0z} + \mu_a k_{2z}} E_0$$

$$E_2 = \frac{2\mu_b k_{0z}}{\mu_a k_{2z} + \mu_b k_{0z}} E_0$$

$$2) \frac{k_{0z}}{\epsilon_a} (H_0 - H_1) = \frac{k_{2z}}{\epsilon_b} H_2$$

solve (1) and (2) for
 H_1 and H_2 in terms of H_0

$$H_1 = \frac{\epsilon_b k_{0z} - \epsilon_a k_{2z}}{\epsilon_b k_{0z} + \epsilon_a k_{2z}} H_0$$

$$H_2 = \frac{2\epsilon_b k_{0z}}{\epsilon_a k_{2z} + \epsilon_b k_{0z}} H_0$$

Define reflection coefficient in terms of the transported energy
 $R = \frac{|E_1|^2}{|E_0|^2} = \frac{|H_1|^2}{|H_0|^2}$

Reflection coefficients

① $\vec{E}_0 \perp$ plane incidence

$$R_{\perp} = \frac{|E_1|^2}{|E_0|^2} = \left| \frac{\mu_b k_{0z} - \mu_a k_{2z}}{\mu_b k_{0z} + \mu_a k_{2z}} \right|^2$$

② $\vec{E}_0 \parallel$ plane incidence

$$R_{\parallel} = \frac{|H_1|^2}{|H_0|^2} = \left| \frac{\epsilon_b k_{0z} - \epsilon_a k_{2z}}{\epsilon_b k_{0z} + \epsilon_a k_{2z}} \right|^2$$

Note: above are correct for an arbitrary medium B

i) Consider region of "total reflection"

$$\Rightarrow \left. \begin{array}{l} \text{Im } \epsilon_b = \epsilon_{b2} \approx 0 \\ \text{Re } \epsilon_b = \epsilon_{b1} < 0 \end{array} \right\} \Rightarrow \vec{k}_2 = i \vec{K}_2 \quad \text{where } \vec{K}_2 \text{ is real} \\ \text{i.e. } \vec{K}_2 \text{ pure imaginary}$$

$$\Rightarrow R_{\perp} = \left| \frac{\mu_b k_{0z} - i \mu_a K_{2z}}{\mu_b k_{0z} + i \mu_a K_{2z}} \right|^2$$

$$R_{\parallel} = \left| \frac{\epsilon_b k_{0z} - i \epsilon_a K_{2z}}{\epsilon_b k_{0z} + i \epsilon_a K_{2z}} \right|^2$$

both are of the form $\left| \frac{a - ib}{a + ib} \right|^2 = 1$ when a, b real

$$\Rightarrow R_{\perp} = R_{\parallel} = 1$$

confirms that the material is completely reflecting

ii) Next consider when medium B is transparent

ϵ_b is real and $\epsilon_b > 0$

$$k_{0z} = \frac{\omega}{c} \sqrt{\mu_a \epsilon_a} \cos \theta_0 = \frac{\omega}{c} \mu_a \cos \theta_0$$

$$k_{2z} = \frac{\omega}{c} \sqrt{\mu_b \epsilon_b} \cos \theta_2 = \frac{\omega}{c} \mu_b \cos \theta_2$$

$$\text{Snell's law holds so } \mu_a \sin \theta_0 = \mu_b \sin \theta_2$$

can write $R_{\perp}$ and $R_{\parallel}$ as functions of θ_0
for simplicity take $\mu_a = \mu_b = 1$

$$\textcircled{1} R_{\perp} = \left(\frac{m_a \cos \theta_0 - m_b \cos \theta_2}{m_a \cos \theta_0 + m_b \cos \theta_2} \right)^2 = \left(\frac{\cos \theta_0 - \left(\frac{\sin \theta_0}{\sin \theta_2} \right) \cos \theta_2}{\cos \theta_0 + \left(\frac{\sin \theta_0}{\sin \theta_2} \right) \cos \theta_2} \right)^2$$

$$= \left(\frac{\sin \theta_2 \cos \theta_0 - \sin \theta_0 \cos \theta_2}{\sin \theta_2 \cos \theta_0 + \sin \theta_0 \cos \theta_2} \right)^2$$

$$R_{\perp} = \left(\frac{\sin(\theta_0 - \theta_2)}{\sin(\theta_0 + \theta_2)} \right)^2$$

for $\theta_0 = 0$, i.e. normal incidence, $\theta_2 = 0$

$$\Rightarrow R_{\perp} = \left(\frac{m_a - m_b}{m_a + m_b} \right)^2 \quad \text{if } m_a = m_b, \text{ no reflection!}$$

(not surprising!)

$$\textcircled{2} R_{\parallel} = \left(\frac{\epsilon_b m_a \cos \theta_0 - \epsilon_a m_b \cos \theta_2}{\epsilon_b m_a \cos \theta_0 + \epsilon_a m_b \cos \theta_2} \right)^2 \quad \text{use } \sqrt{\epsilon_b} = m_b$$

$$\sqrt{\epsilon_a} = m_a$$

$$= \left(\frac{m_b \cos \theta_0 - m_a \cos \theta_2}{m_b \cos \theta_0 + m_a \cos \theta_2} \right)^2$$

$$= \left(\frac{\cos \theta_0 - \left(\frac{\sin \theta_2}{\sin \theta_0} \right) \cos \theta_2}{\cos \theta_0 + \left(\frac{\sin \theta_2}{\sin \theta_0} \right) \cos \theta_2} \right)^2$$

$$= \left(\frac{\sin \theta_0 \cos \theta_0 - \sin \theta_2 \cos \theta_2}{\sin \theta_0 \cos \theta_0 + \sin \theta_2 \cos \theta_2} \right)^2$$

$$R_{\parallel} = \left(\frac{\tan(\theta_0 - \theta_2)}{\tan(\theta_0 + \theta_2)} \right)^2 \quad \leftarrow \text{after some algebra!}$$

for $\theta_0 = 0$, then $\theta_2 = 0$

$$R_{\parallel} = \left(\frac{\epsilon_b m_a - \epsilon_a m_b}{\epsilon_b m_a + \epsilon_a m_b} \right)^2 = \left(\frac{m_b - m_a}{m_b + m_a} \right)^2 \text{ same as } R_{\perp}$$

So for $\theta_0 = 0$, $R_{\parallel} = R_{\perp}$ - this must be so since for $\theta_0 = 0$ there is no distinction between the $\perp$ and $\parallel$ cases

If $m_b = m_a$, $R_{\perp} = R_{\parallel} = 0$ no reflective wave

When $\theta_0 + \theta_2 = \pi/2$, then $\tan(\theta_0 + \theta_2) \rightarrow \infty$
and $R_{\parallel} = 0$

This occurs at an angle of incidence known as Brewster's angle θ_B , determined by

$$\begin{array}{ccc} m_a \sin \theta_B & = & m_b \sin \left(\frac{\pi}{2} - \theta_B \right) = m_b \cos \theta_B \\ \uparrow & & \uparrow \\ \theta_0 & & \theta_2 \end{array}$$

$$\Rightarrow \boxed{\tan \theta_B = \frac{m_b}{m_a}}$$

For incident wave at θ_B , reflected wave always has $\vec{E}_r \perp$ plane of incidence, since $R_{\parallel} = 0$. If incoming wave has $\vec{E}_i \parallel$ plane of incidence, then it gets completely transmitted. If $\vec{E}_i$ in general direction, reflected wave is always linearly polarized with $\vec{E}_r \perp$ plane of incidence. - This is one method to create polarized light wave.