

Boundary value problems in magnetostatics

Scalar Magnetic Potential

Because of the vector character of the equation

$$-\nabla^2 \vec{A} = \frac{4\pi}{c} \vec{j}$$

and the fact that $\nabla^2 \vec{A}$ only has a convenient representation in Cartesian coordinates, many of the methods we used to solve the scalar $-\nabla^2 \phi = 4\pi j$ don't work so well for magnetostatics.

However, in situations where the current \vec{j} is confined to certain surfaces, we can make things much closer to the electrostatic case by using the trick of the scalar magnetic potential ϕ_M .

In regions where $\vec{j} = 0$, i.e. not on the certain surfaces, we have $\vec{\nabla} \cdot \vec{B} = 0$ and $\vec{\nabla} \times \vec{B} = 0$. Since $\vec{\nabla} \times \vec{B} = 0$ in these regions we can define a scalar potential ϕ_M such that

$$\vec{B} = -\vec{\nabla} \phi_M$$

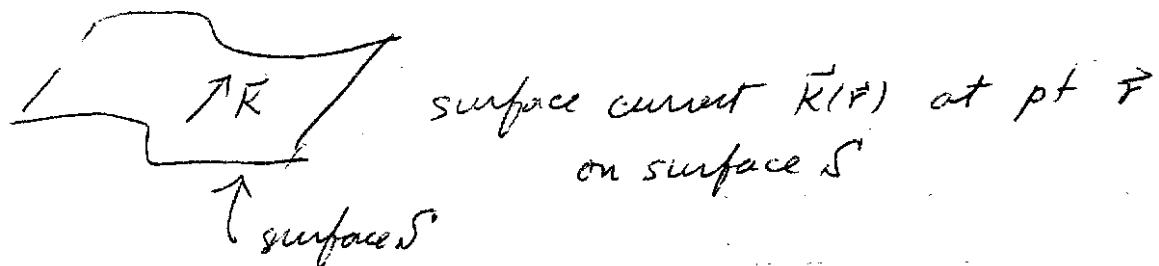
and then

$$\vec{\nabla} \cdot \vec{B} = -\nabla^2 \phi_M = 0$$

We can solve for ϕ_M as in electrostatics, and match solutions by applying appropriate boundary conditions on the current carrying surfaces.

Boundary Conditions at Sheet current

in magnetostatics $\vec{\nabla} \cdot \vec{B} = 0$, $\vec{\nabla} \times \vec{B} = \frac{4\pi}{c} \vec{J}$



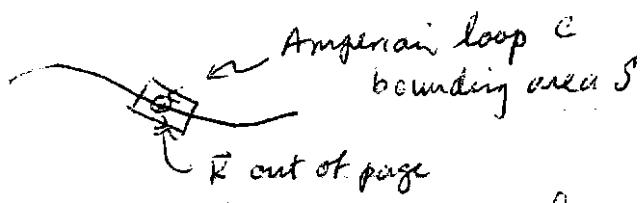
on Gaussian
pillbox vol V $\int_V d^3r \vec{\nabla} \cdot \vec{B} = 0$

side view

top + bottom area of pill box is da
width of pill box $\rightarrow 0$

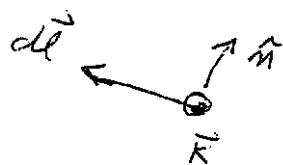
$$\Rightarrow \int_V d^3r \vec{\nabla} \cdot \vec{B} = \oint_S da \hat{n} \cdot \vec{B} = da (\vec{B}_{\text{above}} - \vec{B}_{\text{below}}) \cdot \hat{n} = 0$$

normal component of \vec{B} is continuous $(\vec{B}_{\text{above}} - \vec{B}_{\text{below}}) \cdot \hat{n} = 0$



$$\int_S da \hat{n} \cdot (\vec{\nabla} \times \vec{B}) = \oint_C \vec{B} \cdot d\vec{l} = \frac{4\pi}{c} I_{\text{enclosed}}$$

let width of loop $\rightarrow 0$, top + bottom sides $d\vec{l} \rightarrow$



$$(\vec{B}_{\text{above}} - \vec{B}_{\text{below}}) \cdot d\vec{l} = \frac{4\pi}{c} (K \times \hat{n}) \cdot d\vec{l}$$

$$= \frac{4\pi}{c} (\vec{K} \times \hat{n}) \cdot d\vec{l}$$

\hat{n} is outward
normal

tangential component of \vec{B} has
discontinuous jump $\frac{4\pi}{c} \vec{K} \times \hat{n}$

Combine both results into

$$\boxed{\vec{B}_{\text{above}} - \vec{B}_{\text{below}} = \frac{4\pi}{c} K \times \hat{m}}$$

$$\text{magnetic analog of } \vec{E}_{\text{above}} - \vec{E}_{\text{below}} = 4\pi\sigma \hat{m}$$

In terms of magnetic ~~scalar~~ potential ϕ_M

$$-\vec{\nabla}\phi_{M\text{ above}} + \vec{\nabla}\phi_{M\text{ below}} = \frac{4\pi}{c} K \times \hat{m}$$

Note: ϕ_M is a calculational tool only
it does not have any direct physical
significance as does the electrostatic ϕ .
Electrostatic ϕ is related to work done
moving a charge $W_{12} = q [\phi(r_2) - \phi(r_1)]$
nothing similar for ϕ_M .

(in fact magnetostatic magnetic forces do no work!)

$$\begin{aligned} \vec{F} &= q \vec{\nabla} \times \vec{B} \\ \Rightarrow \vec{F} \cdot \vec{n} &= \frac{dW}{dt} = 0 \end{aligned}$$

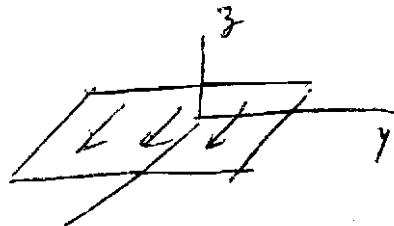
Note: We cannot apply argument $\vec{F} \cdot \vec{n} = \int \vec{B} \cdot d\vec{l}$
 ϕ_M is not necessarily continuous at surface 'current'
Cannot do similar to electrostatics and use
 $\phi_M(r_{\text{above}}) - \phi_M(r_{\text{below}}) = - \int_{r_{\text{below}}}^{r_{\text{above}}} \vec{B} \cdot d\vec{l}$

Since ϕ_M is not defined on the current sheet
itself, separating "above" from "below".

example

Flat infinite plane at $z=0$ with surface current

$$\vec{R} = K \hat{x}$$



$$z > 0, \nabla^2 \phi_M^> = 0 \Rightarrow \phi_M^> = a^> - b_x^> x - b_y^> y - b_z^> z$$

$$z < 0, \nabla^2 \phi_M^< = 0 \Rightarrow \phi_M^< = a^< - b_x^< x - b_y^< y - b_z^< z$$

$$z > 0, \vec{B}^> = -\vec{\nabla} \phi_M^> = b_x^> \hat{x} + b_y^> \hat{y} + b_z^> \hat{z}$$

$$z < 0, \vec{B}^< = -\vec{\nabla} \phi_M^< = b_x^< \hat{x} + b_y^< \hat{y} + b_z^< \hat{z}$$

$$\text{at } z=0 \quad \vec{B}^> - \vec{B}^< = (b_x^> - b_x^<) \hat{x} + (b_y^> - b_y^<) \hat{y} + (b_z^> - b_z^<) \hat{z}$$

$$= \frac{4\pi}{c} \vec{K} \times \hat{m} = \frac{4\pi}{c} K (\hat{x} \times \hat{z}) = -\frac{4\pi}{c} K \hat{y}$$

$$\Rightarrow b_x^> = b_x^< = b_{x0}, \quad b_z^> = b_z^< = b_{z0}, \quad b_y^> - b_y^< = -\frac{4\pi}{c} K$$

define $b_y^> = b_{y0} + \delta b_y \quad \delta b_y = -\frac{2\pi}{c} K$
 $b_y^< = b_{y0} - \delta b_y$

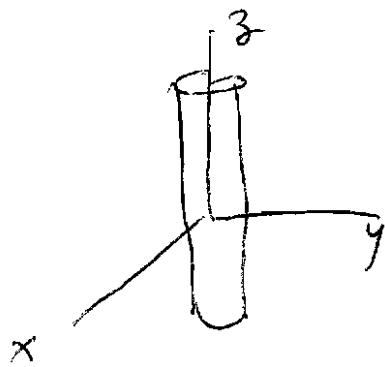
$$\Rightarrow \vec{B}^> = \vec{B}_0 - \frac{2\pi}{c} K \hat{y} \quad \vec{B}_0 = b_{x0} \hat{x} + b_{y0} \hat{y} + b_{z0} \hat{z}$$

$$\vec{B}^< = \vec{B}_0 + \frac{2\pi}{c} K \hat{y}$$

If \vec{K} is the only source of magnetic field then $\vec{B}_0 = 0$

$$\vec{B} = \begin{cases} -\frac{2\pi}{c} K \hat{y} & z > 0 \\ \frac{2\pi}{c} K \hat{y} & z < 0 \end{cases}$$

example current carrying infinite cylinder radius R



- (i) $\vec{K} = K \hat{z}$ wire with surface current
 (ii) $\vec{K} = K \hat{\phi}$ solenoid

(i) $\vec{K} = K \hat{z}$ $2\pi R K = I_{\text{total current}}$
 "guess" + show it is correct

$$r > R \quad \boxed{\Phi_M = -\frac{4\pi}{c} R K \Phi} \quad \text{magnetic scalar potential} \quad \nabla^2 \Phi_M = 0$$

$$r < R \quad \Phi_M = 0$$

$$r > R \quad \vec{B} = -\vec{\nabla} \Phi_M = -\frac{1}{r} \frac{\partial \Phi_M}{\partial \phi} \hat{\phi} = \frac{4\pi R K}{c r} \hat{\phi} = \boxed{\frac{2I}{cR} \hat{\phi}} \quad \leftarrow \text{familiar result from Ampere}$$

$$r < R \quad \vec{B} = 0$$

$$\vec{B}_{\text{above}} - \vec{B}_{\text{below}} = \frac{2I}{cR} \hat{\phi} = \frac{4\pi K}{c} \frac{R}{r} \hat{\phi} = \frac{4\pi K}{c} \vec{r} \times \hat{m}$$

where $\hat{m} = \hat{r}$
 as $\hat{z} \times \hat{r} = \hat{\phi}$

Note: $\Phi_M = -\frac{4\pi}{c} R K \Phi$ is not single valued!
 would not have found this using expansion of separation of coords in polar coords

(iv) $\vec{K} = K \hat{\phi}$

$$r > R \quad \Phi_M = -B_1 \hat{z} \quad \left. \right\} \nabla^2 \Phi_M = 0$$

$$r < R \quad \Phi_M = -B_2 \hat{z}$$

$$r > R \quad \vec{B} = -\vec{\nabla} \Phi_M = B_1 \hat{z}$$

$$r < R \quad \vec{B} = -\vec{\nabla} \Phi_M = B_2 \hat{z}$$

$$\vec{B}_{\text{above}} - \vec{B}_{\text{below}} = (B_1 - B_2) \hat{z} = \frac{4\pi}{2} K \vec{r} \times \hat{m}$$

$$= \frac{4\pi}{2} K (\hat{\rho} \times \hat{r})$$

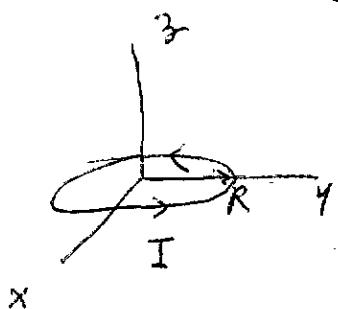
$$= -\frac{4\pi}{2} K \hat{z}$$

If current in solenoid is only source of \vec{B} . Then expect $B_1 = 0$.

$$\Rightarrow \boxed{\vec{B}_2 = \frac{4\pi}{2} K \hat{z}} \quad \text{familiar result}$$

example

circular current loop in xy... plane



$$\text{for } r > R, \vec{\nabla} \times \vec{B} = 0 \Rightarrow \vec{B} = -\vec{\nabla} \phi_M$$

where $\nabla^2 \phi_M = 0$.

Try Legendre polynomial expansion for ϕ_M

$$\phi_M = \sum_{l=0}^{\infty} \frac{B_l}{r^{l+1}} P_l(\cos\theta) \quad (\text{All terms vanish as want } B \rightarrow 0 \text{ as } r \rightarrow \infty)$$

$$\vec{B} = -\vec{\nabla} \phi_M = -\frac{\partial \phi_M}{\partial r} \hat{r} - \frac{1}{r} \frac{\partial \phi_M}{\partial \theta} \hat{\theta}$$

$$= \sum_l \left[\frac{(l+1)B_l}{r^{l+2}} P_l(\cos\theta) \hat{r} - \frac{B_l}{r^{l+2}} \frac{\partial P_l(\cos\theta)}{\partial \theta} \hat{\theta} \right]$$

write $\frac{\partial P_l}{\partial \theta} = \frac{\partial P_l}{\partial x} \cdot \frac{\partial x}{\partial \theta} = -\frac{\partial P_l}{\partial x} \sin\theta \quad x = \cos\theta$

$$= -P'_l \sin\theta$$

$$\vec{B} = \sum_l \left[\frac{(l+1)B_l}{r^{l+2}} P_l(\cos\theta) \hat{r} + \frac{B_l}{r^{l+2}} \sin\theta P'_l(\cos\theta) \hat{\theta} \right]$$

To determine the B_l we compare with exact solution along \hat{z} axis

$$\vec{B}(z\hat{z}) = \sum_l \frac{(l+1)B_l}{r^{l+2}} \hat{r} = \sum_l \frac{(l+1)B_l}{z^{l+2}} \hat{z}$$

Since $P_l(1) = 1$, $\sin(0) = 0$ and $P'_l(1)$ finite, $\hat{r} = \hat{z}$ when $\theta = 0$

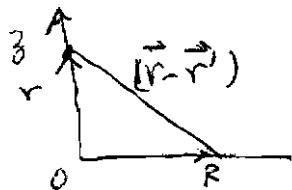
exact solution on \vec{z} axis:

$$\vec{A} = \int_C d^3r' \frac{\vec{f}(r')}{|\vec{r}-\vec{r}'|} \Rightarrow \vec{B}(\vec{r}) = \vec{\nabla} \times \vec{A} = \int_C d^3r' \vec{\nabla} \times \frac{\vec{f}(r')}{|\vec{r}-\vec{r}'|}$$

$$\vec{B} = - \int_C d^3r' \vec{f}(r') \times \vec{\nabla} \left(\frac{1}{|\vec{r}-\vec{r}'|} \right)$$

$$\vec{B} = \int_C d^3r' \vec{f}(r') \times \frac{(\vec{r}-\vec{r}')}{|\vec{r}-\vec{r}'|^3} \quad \text{Biot-Savart Law for magnetostatics}$$

For our loop



$$\vec{B}(z) = \int_0^{2\pi} d\phi \int_C I \hat{\phi} \times \frac{[-R \hat{r} + z \hat{z}]}{(z^2 + R^2)^{3/2}}$$

$$\hat{r} \times \hat{\phi} = \hat{z}$$

$$= \int_0^{2\pi} d\phi \int_C \frac{R(I R) \hat{z}}{(z^2 + R^2)^{3/2}}$$

$\hat{\phi} \times \hat{z}$ term
integrated to zero

$$\boxed{\vec{B}(z) = \frac{2\pi R^2 I \hat{z}}{c(z^2 + R^2)^{3/2}}}$$

to match Legendre polynomial expansion, do Taylor series expansion of above

$$\vec{B}(z) = \frac{2\pi R^2 I \hat{z}}{c z^3} \frac{1}{(1 + (\frac{R}{z})^2)^{3/2}} = \frac{2\pi R^2 I \hat{z}}{z^3} \left\{ 1 - \frac{3}{2} \left(\frac{R}{z}\right)^2 + \dots \right\}$$

$$= \frac{2\pi R^2 I \hat{z}}{c} \left\{ \frac{1}{z^3} - \frac{3}{2} \frac{R^2}{z^5} + \dots \right\}$$

$$\Rightarrow \left\{ \frac{B_0}{z^2} + \frac{2B_1}{z^3} + \frac{3B_2}{z^4} + \frac{4B_3}{z^5} + \dots \right\} \hat{z}$$

$$\Rightarrow B_0 = 0, \quad B_1 = \frac{\pi R^2 I}{c} \hat{I}, \quad B_2 = 0, \quad B_3 = -\frac{3 \pi R^2 I R^2}{4c}$$

So to order $L=3$

$$\vec{B}(r) = \frac{\pi R^2 I}{c} \left\{ \frac{2 P_1(\cos\theta) \hat{r} + \sin\theta P_1'(\cos\theta) \hat{\theta}}{r^3} - \frac{[3R^2 P_3(\cos\theta) \hat{r} + \frac{3}{4} R^2 \sin\theta P_3'(\cos\theta) \hat{\theta}]}{r^5} + \dots \right\}$$

$$P_1(x) = x \Rightarrow P_1'(x) = 1$$

$$P_3(x) = \frac{1}{2}(5x^3 - 3x) \Rightarrow P_3'(x) = \frac{1}{2}(15x^2 - 3)$$

$$\vec{B}(r) = \frac{\pi R^2 I}{c} \left\{ \frac{2 \cos\theta \hat{r} + \sin\theta \hat{\theta}}{r^3} - \frac{\frac{3}{2} R^2 (5 \cos^3\theta - 3 \cos\theta) \hat{r} + \frac{3}{8} R^2 \sin\theta (15 \cos^2\theta - 3) \hat{\theta}}{r^5} \right\} + \dots$$

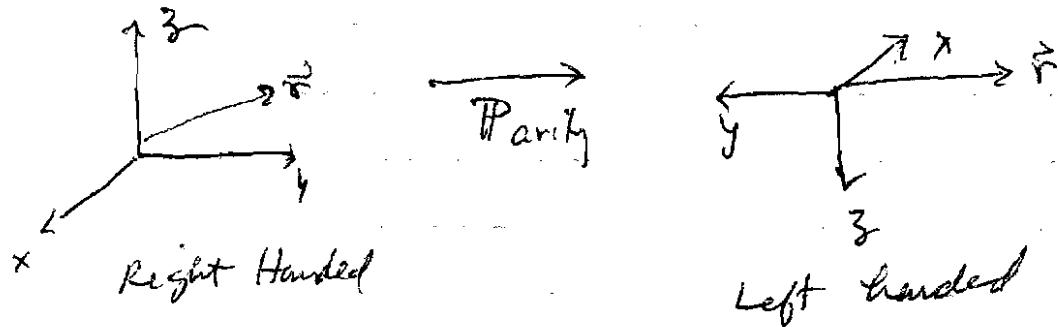
$\frac{\pi R^2 I}{c} = m$ is the magnetic dipole moment of the loop

We see that the 1st term is just the magnetic dipole approx. The 2nd term is the magnetic octupole term. Could easily get higher order terms by this method.

Compare our result above to Jackson (5-40)

Symmetry under parity transformation

vector vs. pseudovector



$$\vec{r} = (x, y, z) \rightarrow (-x, -y, -z)$$

$$P(\vec{r}) = -\vec{r} \quad \text{position } \vec{r} \text{ is odd under parity}$$

Any vector-like quantity that is odd under P is a vector.

examples of vectors

position \vec{r}

velocity $\vec{v} = \frac{d\vec{r}}{dt}$ since \vec{r} is vector and t is scalar

acceleration $\vec{a} = \frac{d\vec{v}}{dt}$

$$P(t) = t$$

Force $\vec{F} = m\vec{a}$

since \vec{a} is vector and m is scalar

momentum $\vec{p} = m\vec{v}$

since \vec{v} is vector and m is scalar

electric field $\vec{E} = q\vec{E}$

since \vec{E} is vector and q is scalar

current $\vec{j} = \sum_j j_i \vec{v}_i \delta(\vec{r} - \vec{r}_i(t))$

$$P(q) = q$$

any vector-like quantity that is even under P is a pseudovector

angular momentum $\vec{L} = \vec{r} \times \vec{p}$ since $\vec{r} \rightarrow -\vec{r}$ and $\vec{p} \rightarrow \vec{p}$,
 $\vec{L} \rightarrow \vec{L}$ under P

magnetic field $\vec{F} = g \vec{v} \times \vec{B}$ since \vec{F} and \vec{v} are vectors and
 g is scalar, \vec{B} must be pseudovector,

cross product of any two vectors is a pseudovector

" " " vector ad pseudovector is a vector

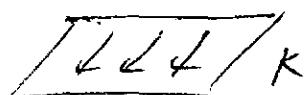
when solving for \vec{E} , it can only be made up of
vectors that exist in the problem

when solving for \vec{B} , it can only be made up of
pseudovectors that exist in the problem

\Rightarrow charged plane



surface current



only directions in problem is normal \hat{m}
 \hat{m} is a vector

$$\vec{E} \propto \hat{m}$$

only directions are the vectors \hat{m} ad \vec{K} . But \vec{B} can only be made of
pseudovectors

$$\Rightarrow \vec{B} \propto (\vec{k} \times \hat{m})$$