

## Momentum Conservation

For charges  $q_i$  at positions  $\vec{r}_i$  with velocities  $\vec{v}_i$

$$\frac{d\vec{P}^{\text{mech}}}{dt} = \sum_i \vec{F}_i = \sum_i q_i (\vec{E}(\vec{r}_i) + \frac{1}{c} \vec{v}_i \times \vec{B}(\vec{r}_i))$$

$\uparrow$   
 "mechanical"  
 momentum of  
 the charges

$\uparrow$   
 force on  
 charge  $i$

$$= \int_V d^3r \left[ \rho \vec{E} + \frac{1}{c} \vec{j} \times \vec{B} \right]$$

$$\rho \vec{E} + \frac{1}{c} \vec{j} \times \vec{B} = \frac{1}{4\pi} \left[ \vec{E} (\vec{\nabla} \cdot \vec{E}) + (\vec{\nabla} \times \vec{B} - \frac{1}{c} \frac{\partial \vec{E}}{\partial t}) \times \vec{B} \right]$$

Now  $\frac{1}{c} \frac{\partial}{\partial t} (\vec{E} \times \vec{B}) = \frac{1}{c} \left( \frac{\partial \vec{E}}{\partial t} \times \vec{B} \right) + \frac{1}{c} \left( \vec{E} \times \frac{\partial \vec{B}}{\partial t} \right)$  use  $\vec{\nabla} \times \vec{E} = -\frac{1}{c} \frac{\partial \vec{B}}{\partial t}$

$$= \frac{1}{c} \left( \frac{\partial \vec{E}}{\partial t} \times \vec{B} \right) - \vec{E} \times (\vec{\nabla} \times \vec{E})$$

So  $-\frac{1}{c} \frac{\partial \vec{E}}{\partial t} \times \vec{B} = -\vec{E} \times (\vec{\nabla} \times \vec{E}) - \frac{1}{c} \frac{\partial}{\partial t} (\vec{E} \times \vec{B})$

Therefore

$$\rho \vec{E} + \frac{1}{c} \vec{j} \times \vec{B} = \frac{1}{4\pi} \left[ \vec{E} (\vec{\nabla} \cdot \vec{E}) + \vec{B} (\vec{\nabla} \cdot \vec{B}) - \vec{B} \times (\vec{\nabla} \times \vec{B}) - \vec{E} \times (\vec{\nabla} \times \vec{E}) - \frac{1}{c} \frac{\partial}{\partial t} (\vec{E} \times \vec{B}) \right]$$

Define electromagnetic momentum density

$$\vec{\Pi} = \frac{1}{4\pi c} \vec{E} \times \vec{B} = \frac{1}{c^2} \vec{S} \quad (\vec{S} \text{ is Poynting vector})$$

then

$$\frac{d\vec{P}^{\text{mech}}}{dt} + \frac{d}{dt} \int_V d^3r \vec{\Pi} = \frac{1}{4\pi} \int_V d^3r \left[ \vec{E} (\vec{\nabla} \cdot \vec{E}) - \vec{E} \times (\vec{\nabla} \times \vec{E}) + \vec{B} (\vec{\nabla} \cdot \vec{B}) - \vec{B} \times (\vec{\nabla} \times \vec{B}) \right]$$

want to rewrite as a surface integral

$i$ th component of integrand on right hand side is ( $\vec{E}$  part only)  
(sum over repeated indices)

$$\begin{aligned} & E_i \partial_j E_j - \epsilon_{ijk} E_j \epsilon_{klm} \partial_l E_m \\ &= E_i \partial_j E_j - (\delta_{il} \delta_{jm} - \delta_{im} \delta_{jl}) E_j \partial_l E_m \\ &= E_i \partial_j E_j - E_j \partial_i E_j + E_j \partial_j E_i \\ &= \partial_j (E_i E_j - \frac{1}{2} \delta_{ij} E^2) \end{aligned}$$

Define Maxwell's stress tensor

$$T_{ij} = \frac{1}{4\pi} [E_i E_j + B_i B_j - \frac{1}{2} \delta_{ij} (E^2 + B^2)]$$

(note  $T_{ij} = T_{ji}$   
Symmetric tensor)

Then

$$\frac{d}{dt} \vec{p}_i^{\text{mech}} + \frac{d}{dt} \int_V d^3r \Pi_i = \int_V d^3r \partial_j T_{ij} \quad \left( \partial_j T_{ij} = \frac{\partial T_{ij}}{\partial x_j} \right)$$

$$= \oint_S da T_{ij} \cdot \hat{n}_j$$

$$\frac{d}{dt} \vec{p}^{\text{mech}} + \frac{d}{dt} \int_V d^3r \vec{\Pi} = \oint_S da \vec{T} \cdot \hat{n}$$

-  $T_{ij}$  gives the flow of the  $i$ th component of electromagnetic field momentum through an element of surface area  $da$  to direction  $\hat{e}_j$

For static situations where  $\frac{d\Pi}{dt} = 0$ ,  $\frac{d\vec{p}^{\text{mech}}}{dt} = \vec{F}_{\text{tot}} = \oint_S da \vec{T} \cdot \hat{n}$   
Gives electromagnetic force on the surface  $S$

Note:  $\frac{d\vec{P}^{\text{mech}}}{dt}$  is ~~also~~ equal to the total electromagnetic force on the volume  $V$ .

Hence we can write

$$\vec{F}_{EM} = \oint_S da \vec{T} \cdot \hat{n} - \frac{d}{dt} \int_V d^3r \vec{\Pi}$$

for static situations, the 2<sup>nd</sup> term vanishes and

$$\vec{F}_{EM} = \oint_S da \vec{T} \cdot \hat{n}$$

$T_{ij}$  is the  $ij$ th component of static force on unit area with normal  $\hat{e}_j$ .

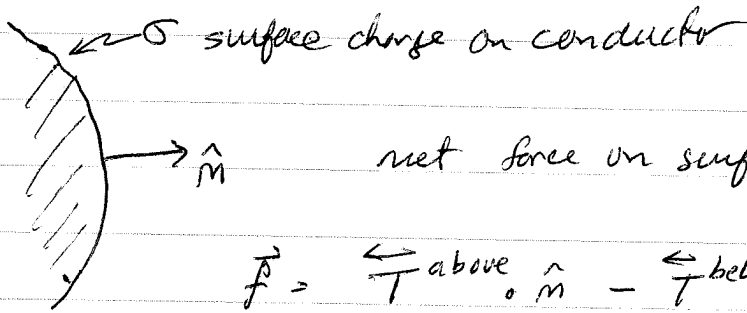
this is origin of the term "stress" tensors.

$\vec{T}$  is like the stress tensor of an elastic medium.

$T_{xx}, T_{yy}, T_{zz}$  are like pressure.

off diagonal elements are like shear stresses

## Force on a conductor surface,



net force on surface per unit area is

$$\vec{f} = \vec{T}^{\text{above}} \cdot \hat{n} - \vec{T}^{\text{below}} \cdot \hat{n}$$

$\uparrow = 0$  as  $\vec{E} = 0$  inside conductor

$$\vec{f} = \frac{1}{4\pi} \left[ \vec{E} (\vec{E} \cdot \hat{n}) - \frac{1}{2} \hat{n} E^2 \right]$$

for conducting surface

$$\hat{n} \cdot \vec{E}^{\text{above}} = 4\pi\sigma \quad (\text{since } \vec{E}^{\text{below}} = 0)$$

and tangential component  $\vec{E} = 0$

$$\Rightarrow \vec{E} = 4\pi\sigma \hat{n}$$

$$\text{So } \vec{f} = \frac{1}{4\pi} \left[ (4\pi\sigma \hat{n})(4\pi\sigma) - \frac{1}{2} \hat{n} (4\pi\sigma)^2 \right]$$

$$\vec{f} = \frac{1}{4\pi} \left[ (4\pi\sigma)^2 \hat{n} - \frac{1}{2} (4\pi\sigma)^2 \hat{n} \right]$$

$$\vec{f} = \frac{\hat{n}}{4\pi} \left[ (4\pi\sigma)^2 - \frac{1}{2} (4\pi\sigma)^2 \right] = 2\pi\sigma^2 \hat{n}$$

force per unit area:

$$\vec{f} = 2\pi\sigma^2 \hat{n} = \frac{1}{2} \sigma \vec{E}$$

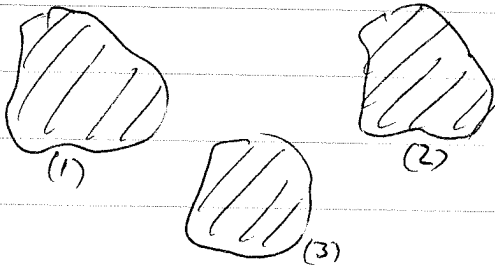
$$\vec{f} = \sigma \vec{E}_{\text{ave}}$$

where  $\vec{E}_{\text{ave}} = \frac{1}{2} (\vec{E}^{\text{above}} + \vec{E}^{\text{below}})$   
is average field at surface  
averaging over above + below

Note factor  $\frac{1}{2}$ . Naively one might have thought  $\vec{f} = \sigma \vec{E}$ . But need to exclude self field of charge on surface from acting on itself. See also Jackson pg 42 for another approach.

# Capacitance

Consider a set of conductors with potential  $\phi(\vec{r}) = V_i$  fixed on conductor  $i$



(also need condition on  $\phi(\vec{r}) \rightarrow \infty$  if system is not enclosed)

From uniqueness theorem we know that specifying the  $V_i$  on each conductor is enough to determine the potential  $\phi(\vec{r})$  everywhere. We can write this potential in the following form -

Let  $\phi^{(i)}(\vec{r})$  be the solution to the boundary value problem  $\nabla^2 \phi^{(i)}(\vec{r}) = 0$  and  $\phi^{(i)}(\vec{r}) = \begin{cases} 1 & \text{if } \vec{r} \text{ on surface of conductor } (i) \\ 0 & \text{if } \vec{r} \text{ on surface of any other conductor } (j), j \neq i \end{cases}$

Then by superposition

$$\phi(\vec{r}) = \sum_i V_i \phi^{(i)}(\vec{r})$$

is solution to the problem  $\nabla^2 \phi = 0$  and  $\phi(\vec{r}) = V_i$  for  $\vec{r}$  on surface of conductor  $(i)$

The surface charge density at  $\vec{r}$  on surface of conductor  $(i)$  is

$$\sigma^{(i)}(\vec{r}) = \frac{-1}{4\pi} \frac{\partial \phi(\vec{r})}{\partial n} = -\frac{1}{4\pi} \sum_j V_j \frac{\partial \phi^{(j)}(\vec{r})}{\partial n}$$

where  $\frac{\partial \phi}{\partial n} = (\vec{\nabla} \phi) \cdot \hat{n}$  is the derivative normal to the surface at point  $\vec{r}$ .

The total charge on conductor (i) is

$$Q_i = \int_{S_i} da \sigma^{(i)}(\vec{r}) = -\frac{1}{4\pi} \sum_j V_j \int_{S_i} da \frac{\partial \phi^{(j)}}{\partial n}$$

↑  
surface of conductor (i)

Define  $C_{ij} \equiv -\frac{1}{4\pi} \int_{S_i} da \frac{\partial \phi^{(j)}}{\partial n}$

the  $C_{ij}$  depend only on the geometry of the conductors

Then we have

$$Q_i = \sum_j C_{ij} V_j$$

↑

$C_{ij}$  is the capacitance matrix

The charge on conductor (i) is a linear function of the potentials  $V_j$  on the conductors (j)

Since we know that specifying the  $Q_i$  that is on each conductor will uniquely determine  $\phi(\vec{r})$  and hence the potential  $V_i$  on each conductor, the capacitance matrix is invertible

$$V_i = \sum_j [C^{-1}]_{ij} Q_j$$

The electrostatic energy of the conductors is then

$$E = \frac{1}{2} \int d^3r \rho \phi = \frac{1}{2} \sum_i Q_i V_i = \frac{1}{2} \sum_{i,j} C_{ij} V_i V_j = \frac{1}{2} \sum_{i,j} C_{ij}^{-1} Q_i Q_j$$

Common to define Capacitance of two conductors by

$$C = \frac{Q}{V_1 - V_2}$$

when conductor (1) has charge  $Q$   
conductor (2) has charge  $-Q$

$V_1 - V_2$  is potential difference between the two conductors.

all other conductors fixed at  $V_i = 0$

We can determine  $C$  in terms of the elements of the matrix  $C_{ij}$

$$\left. \begin{aligned} Q &= C_{11}V_1 + C_{12}V_2 \\ -Q &= C_{21}V_1 + C_{22}V_2 \end{aligned} \right\} \Rightarrow V_2 = -\left(\frac{C_{11} + C_{21}}{C_{12} + C_{22}}\right)V_1$$

$$\Rightarrow Q = \left[ C_{11} - C_{12} \left( \frac{C_{11} + C_{21}}{C_{12} + C_{22}} \right) \right] V_1$$

$$V_1 - V_2 = \left[ 1 + \left( \frac{C_{11} + C_{21}}{C_{12} + C_{22}} \right) \right] V_1$$

$$C = \frac{Q}{V_1 - V_2} = \frac{C_{11} - C_{12} \left( \frac{C_{11} + C_{21}}{C_{12} + C_{22}} \right)}{1 + \left( \frac{C_{11} + C_{21}}{C_{12} + C_{22}} \right)}$$

$$C = \frac{C_{11}C_{22} - C_{12}C_{21}}{C_{11} + C_{12} + C_{21} + C_{22}}$$

Capacitance can also be defined when the space between the conductors is filled with a dielectric  $\epsilon$ . In this case, if  $Q_i$  is the free charge, then  $Q_i/\epsilon$  is the effective total charge to use in computing  $\phi$ .

$$\Rightarrow \frac{Q_i}{\epsilon} = \sum_j C_{ij}^{(0)} V_j$$

where  $C_{ij}^{(0)}$  are capacitances appropriate to a vacuum between the conductors

$$\Rightarrow Q_i = \sum_j \epsilon C_{ij}^{(0)} V_j$$

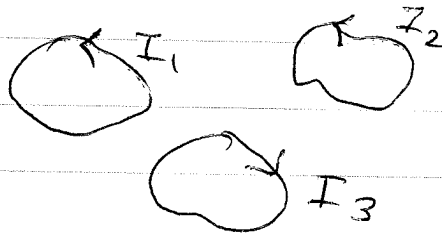
$$= \sum_j C_{ij} V_j \quad \text{where } C_{ij} = \epsilon C_{ij}^{(0)}$$

the capacitance is increased by a factor the dielectric constant  $\epsilon$ .



## Inductance

Consider a set of current carrying loops  $C_i$  with currents  $I_i$



In Coulomb gauge, we can write the magnetic vector potential  $\vec{A}$  from these current loops as

$$\vec{A}(\vec{r}) = \frac{1}{c} \int d^3r' \frac{\vec{j}(\vec{r}')}{|\vec{r} - \vec{r}'|} = \sum_i \frac{I_i}{c} \oint_{C_i} \frac{d\vec{l}'}{|\vec{r} - \vec{r}'|}$$

↑ integrate over loop  $C_i$   
integration variable is  $\vec{r}'$

The magnetic flux through loop  $i$  is

$$\Phi_i = \int_{S_i} da \hat{n} \cdot \vec{B} = \int_{S_i} da \hat{n} \cdot \vec{\nabla} \times \vec{A} = \oint_{C_i} d\vec{l} \cdot \vec{A}$$

↑ surface bounded by loop  $C_i$

$$\Phi_i = \sum_j \frac{I_j}{c} \oint_{C_i} \oint_{C_j} \frac{d\vec{l}_i \cdot d\vec{l}_j}{|\vec{r}_i - \vec{r}_j|}$$

pure geometrical quantity

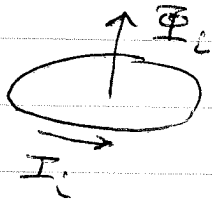
$$\boxed{\Phi_i \equiv c \sum_j M_{ij} I_j}$$

$$\text{where } M_{ij} = \oint_{C_i} \oint_{C_j} \frac{d\vec{l}_i \cdot d\vec{l}_j}{c^2 |\vec{r}_i - \vec{r}_j|}$$

is the mutual inductance of loops  $(i)$  and  $(j)$ .  $M_{ji} = M_{ij}$

$L_i \equiv M_{ii}$  is self-inductance of loop (i)

The sign convention in the above is that,  $\Phi_i$  is computed in direction given by right hand rule, according to the direction taken for current in loop (i)



Magnetostatic energy

$$\mathcal{E} = \frac{1}{2c} \int d^3r \vec{j} \cdot \vec{A} = \frac{1}{2c} \sum_i \oint_{C_i} d\vec{l} \cdot \vec{A} I_i$$

$$= \frac{1}{2c} \sum_i \Phi_i I_i$$

$$\mathcal{E} = \frac{1}{2} \sum_{i,j} M_{ij} I_i I_j$$