

# Hexagonal Design for MINERvA

## A. Bodek- Assembly procedure

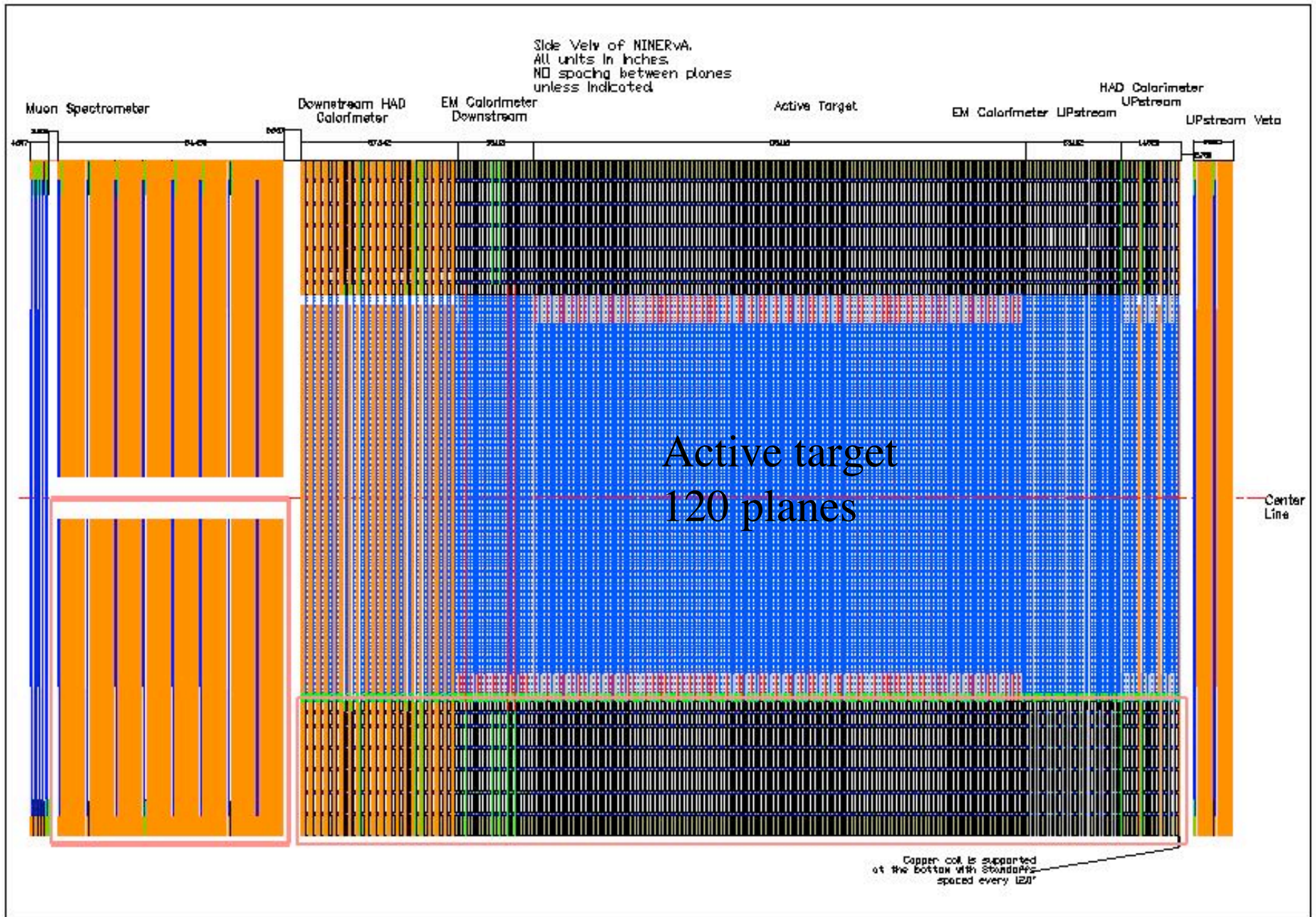
### 11/22/03 and Cost Estimate

Use figures from <http://www.pas.rochester.edu/~teng/>

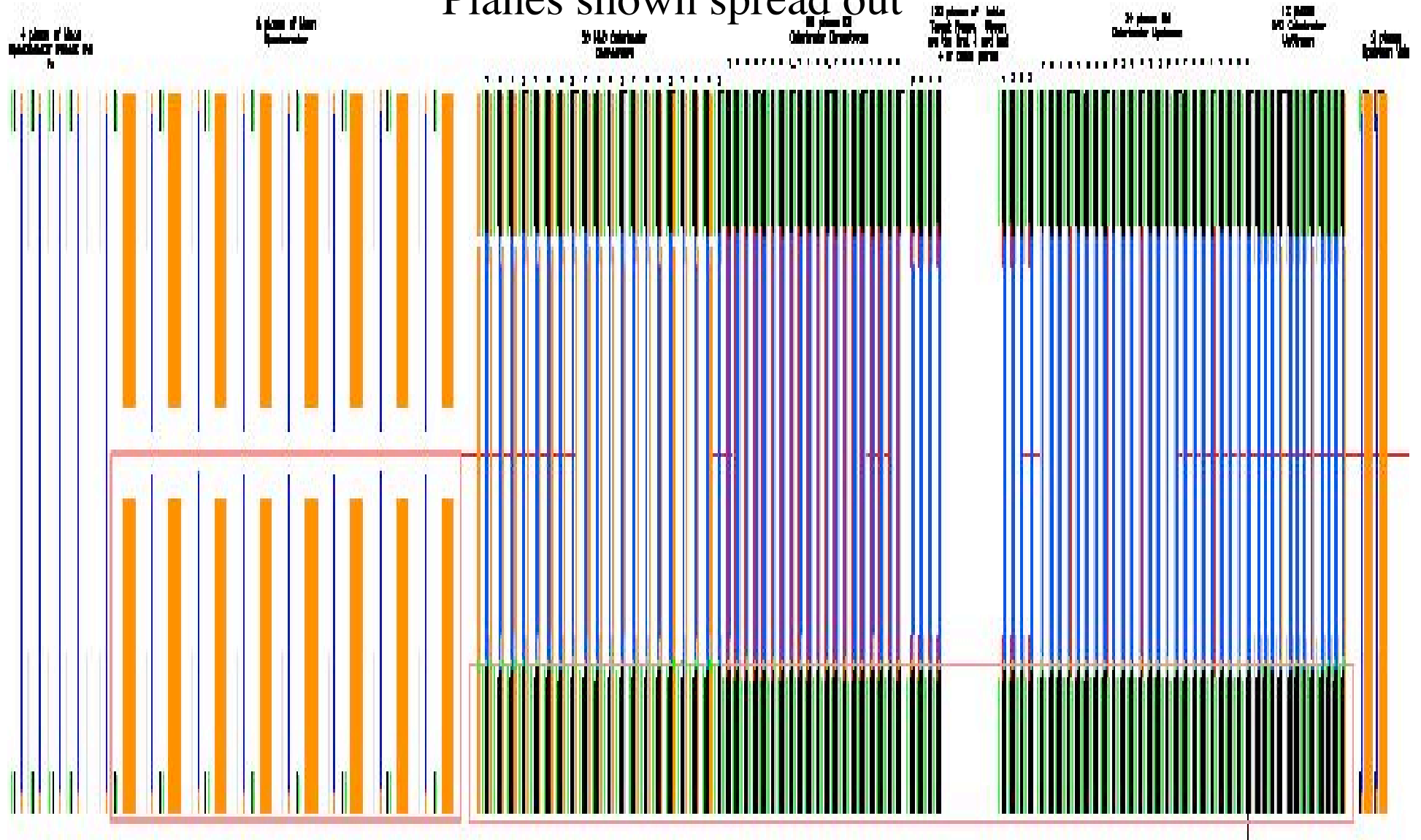
Click on MINERvA/ click on : acwebpublish.htm

- (1) Define: Superplane or Supermodule. 4 planes together XUXV.
- (2) Define a single plane as one of these.
- (3) Start with Parts list and Assembly procedure. Constrain all work to be completed in one year (6 months for 120 planes of active target and barrel).
- (4) This defines space considerations and number of techs.
- (5) Use Active Target+Plus barrel calorimeter (120 planes) as a benchmark for construction.
- (6) For now, multiply by 2 to get total assembly time (to account for hadron calorimeter, muon spectrometer and upstream vetos (later refine costs more exactly for those))

# ASSUMING NO SPACE BETWEEN PLANES



# Planes shown spread out



## **Slide 4: Start with rough estimate then refine as we define detailed procedure:**

**Take a plane with 128 active bars in the inner plus  $+6 \times 8$  (outer/barrel) detector =  $128 + 48 = 172$  bars**

**Assume: 6 8-channel connectors for barrel and 8 16-channel connectors (4 for left side and 4 for right side).**

**Assume that one needs 2 people to lift bars and install in place and route to connector. Assume average of 12 bars per hour (about 5 min a bar) for two people.**

**$172 \text{ bars}/12 = 14 \text{ hours}$ . So with 7 hours a day, one gets one plane per 2 days. Assume that we have 2 tables in parallel, so we have 2 planes per two days (with 4 people). This takes 120 days, or six months with 4 techs (plus one tech to help prepare the next table and assembly supermodules.**

**$120 \text{ planes} = 120 \times 172 = 20,640 \text{ channels}$ .**

## **Slide 5: Estimate of rest of detector.**

**If active detector 120 planes take 6 months with 5 techs for 20K channels.**

**Assume that the other 15K channels plus prototyping (for muon absorber, hadron calorimeter etc,. takes another six months,**

**Get 5 techs for one year for assembly of all supermodules.**

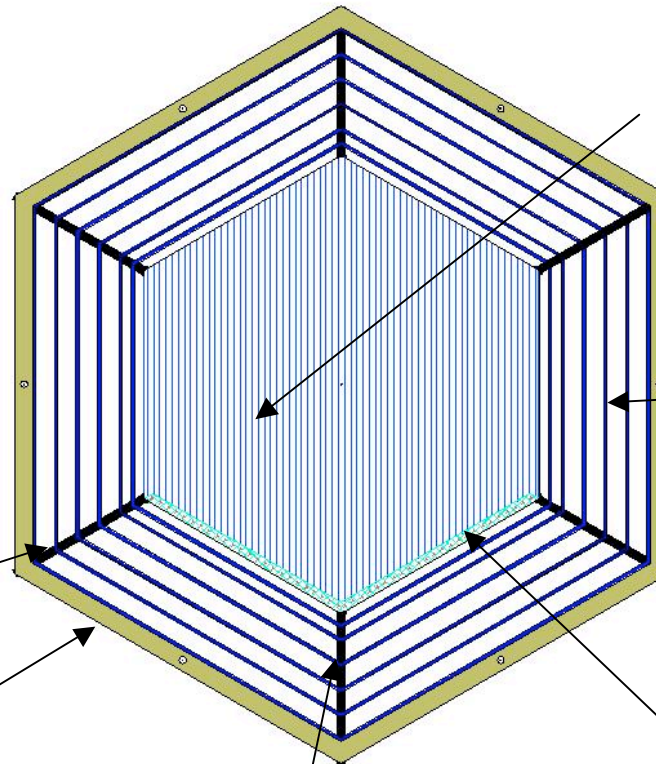
**At \$75K per tech per year (including benefits, overhead) times 5. This is about \$375K.**

**We get 5 tech for one year total.**

**Now we see if our estimate of 5 techs for 6 months for 120 planes, with two parallel setup tables is reasonable if we go through all the details.**

## Slide 6: PLANE Parts P1, C1, C2, G1

**P1. Steel hexagon frame. All welded together to six steel spokes which are 1.7 cm wide (thickness about 1 cm)**



C1.(1- 64), 128  
counters total  
active target

C2.(1- 8)  
48  
counters total  
In barrel

P1.1.  
10 cm external  
Structural frame

P1.2  
6 spokes

G1.1 2 G10  
bars with 24  
holes for coils.  
Screwed to  
first steel bar



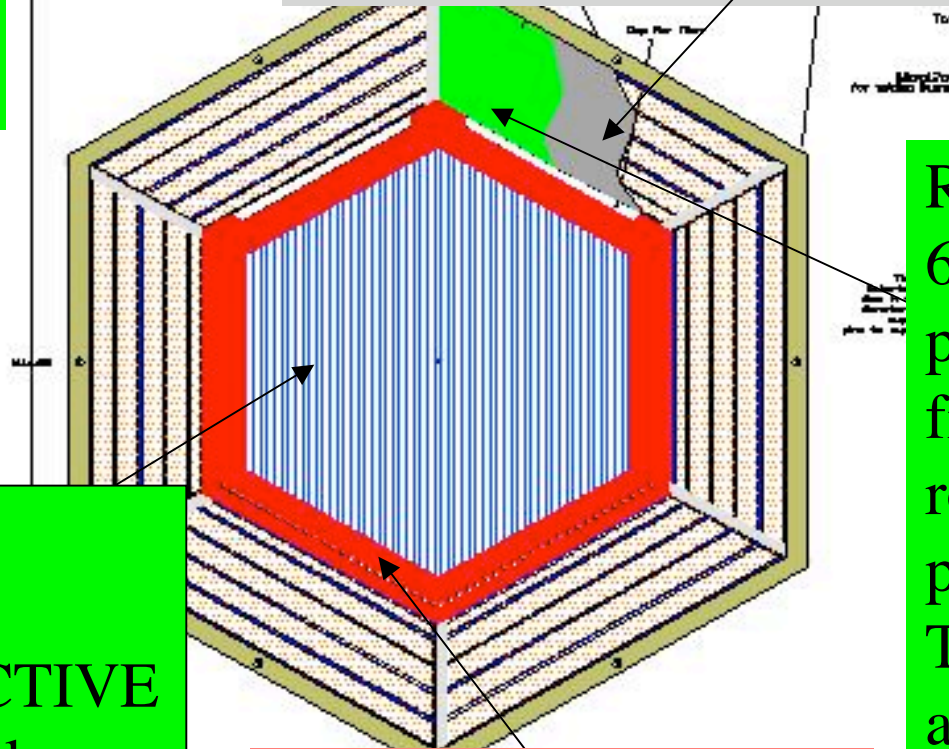


Note: Layer B2 in NuTeV was Marvelguard. It was Tyvek + Tedlar in CMS

**Slide 8: PLANE**  
**Front**  
**Parts L1, R1, S2, B2**

B2 (not shown) thin Light tight & protective Layer covering only ACTIVE layer of hexagon and below L1 (held in place by L1).  
□ Either marvelguard, or a Layer of Tyvek-white house wrap and Tedlar on outside (black plastic)

S2 6 {2-mm G10 or Al or stainless steel 0.25 mm } to protect Routing plate R1



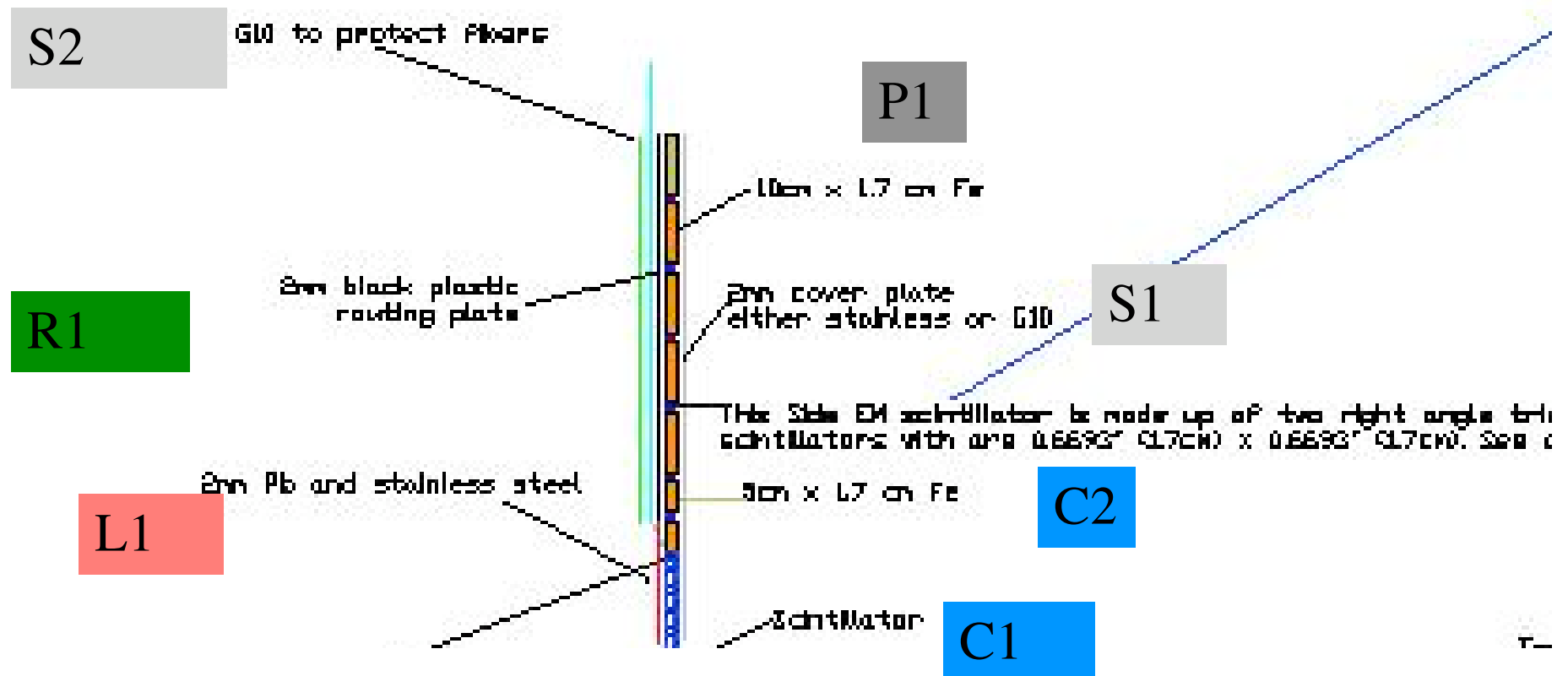
R1.(1-3)  
6 Black plastic fiber routing plates. Top 2 are different from bottom 4

L1. 1.5 mm lead sandwiched between 0.25 mm Stainless flat screwed to first steel bar



Slide 9: Note- thicknesses and materials need to be updated on drawing. B1 and B2 protective layers not shown

### X-Section of Active Target



**Slide 10: Step 1 P1->P1A:** {P1 is the Steel Hexagon Frame, welded together to make a Hexagon. 8 Hexagon bars welded together along six spokes to keep their separation from each other (a small dead area) (one per plane) - Function, Hadron calorimeter, barrel muon detector (magnetized).}. P1 units are stored vertically and can be moved and layed down without any backing, Have one P1 on table 1, and one P1 on table 2. Each day. Each table has a backing fixture on it for lifting final assembled plane later. The P1A (is P1 with backing) is constructed as follows.

- (a) Start with P1 on table. Flat screw two 10 cm G1 bars with 24 holes each in them (G1 used for coil positioning) to bottom two inner sides of steel bars of hexagon.
- (b) Put thin protective layer over B1 over entire hexagon.
- (c) Flat screw six units of S1 (2 with holes which cover G1 bars and 4 without holes over rest of hexagon. P1A is now complete.
- (d) Pick up P1A (which has the back side up) with crane and flip over so P1A back side is down.

**Assume counters are extruded with white light tight skins and have Fibers in them. Already in assembly area.**

## **Slide 11: Step 2 inserting counters: Subunit P1B**

**Assume R1 covers plates have connectors on them and fiber grooves.**

- (a) Put counters C2. (1-8) in each inter steel gaps in the barrel**
- (b) Repeat for all remaining 5 barrel sections of hexagon (two 2-man team working in parallel,**
- (c) Put Readout Cover Plates R1. (1.-6) over barrel sections and flat screw to steel bars in barrel.**
- (d) Run fibers from Barrel in groove of R1 readout plate and insert into the six 8-fiber connectors. Light tight with tape all areas.**
- (e) Start on one edge and put active counters C1 one at a time into the frame. And rout fiber in groove to each of the four 16-fiber connectors. Complete left half (64 counters) one team while second team does right half. Put tape over grooves to light tight and place fibers in place**
- (f) Put light&protective layer B2 over entire area of 128 active counters.**
- (g) Light tight all areas between layer B2 and cover plate R1**

## **Slide 12: Step 3 putting on lead and final assembly: Subunit P1C**

- (a) Put epoxy into connectors to glue connectors to fibers. Plane should now be light tight.
- (b) Put protective cover S2 over six Readout cover plates R1.(1-6)and flat screw to steel, Flat screws must be large to transfer force to steel bar. There are round washers in the holes R1 so that no pressure is put on the fibers and R1 if plate S2 is hit.
- (b) Take lead sheet which backed by stainless steel on each side and put on the counters. Flat screw to steel bars.
- (c) Wait for epoxy to cure overnight.

**In parallel, plane 2 which cured the night before has connectors cut and polished with portable diamond unit.**

- (b) Move over to table 2 which has a plane from last night.
- (a) Attach plane to backup lifting gig with bolts to steel frame
- (b) Lift plane with crane, bring over to storage area. Remove backup lifting gig, and attach to Supermodule (XUXV) with bolts
- (c) Assume that supermodule of 4 planes, with steel backing on the sides is 10 cm thick and can be lifted and transported vertically safely later.

# Old Presentation --Hexagonal Design for MINERvA

A. Bodek, Updated Nov. 14, 2003

1. Designed to be movable to off axis tunnel (less than 4.4 meter in transverse dimensions)
2. Designed to have  $X_u X_v$  segmentation
3. All fiber routing and mechanical design considerations understood
4. Have sufficient side magnetic field for full solid angle muon sign and momentum determination for off axis (low energy running) - For on axis, it helps to be in front of MINOS to improve resolution of high E forward muons
5. Excellent EM resolution, reasonable hadron resolution

# OLD-Hexagonal Design file for MINERvA

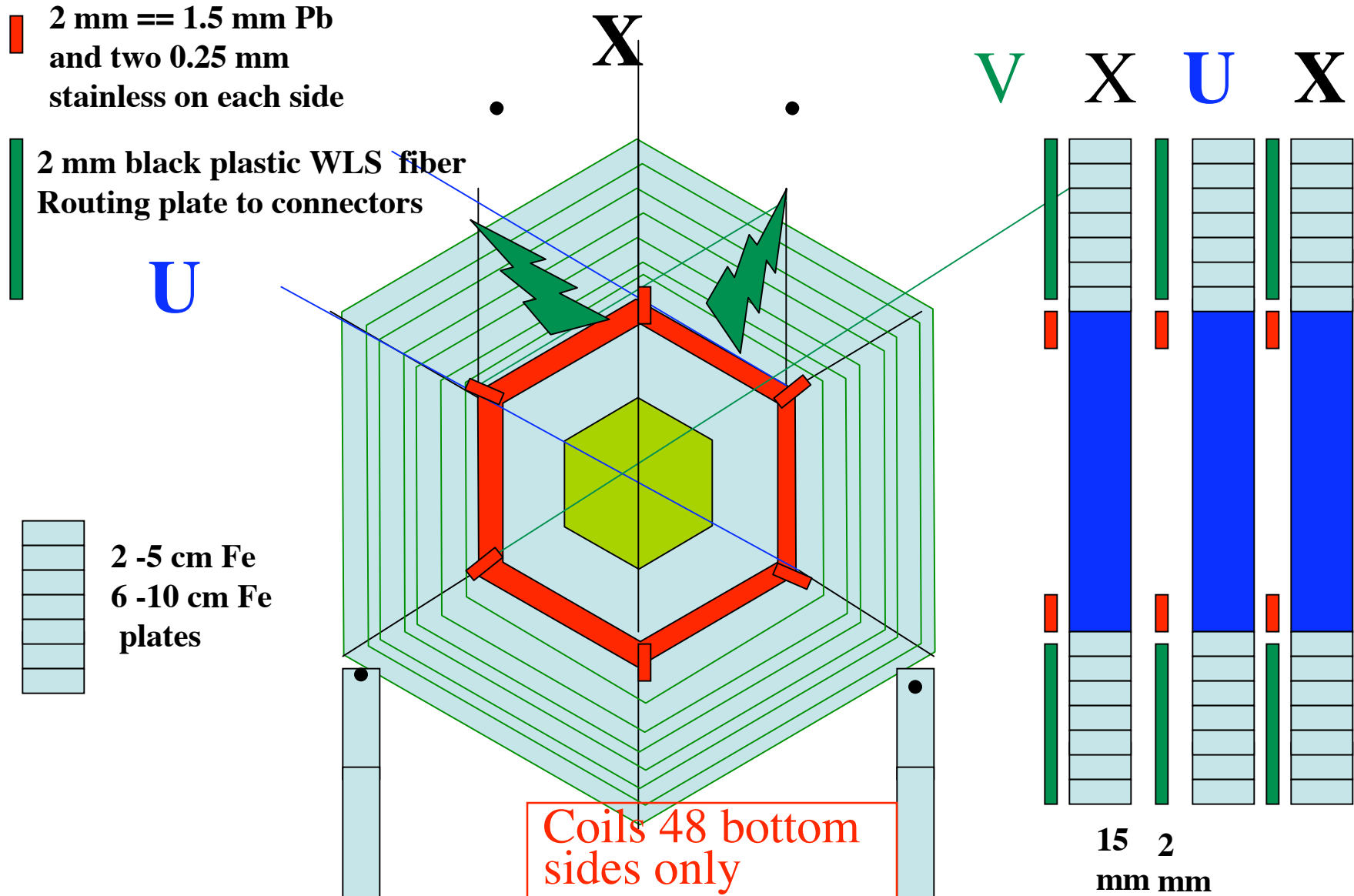
A. Bodek, Nov. 14, 2003

Things that still need to be done:

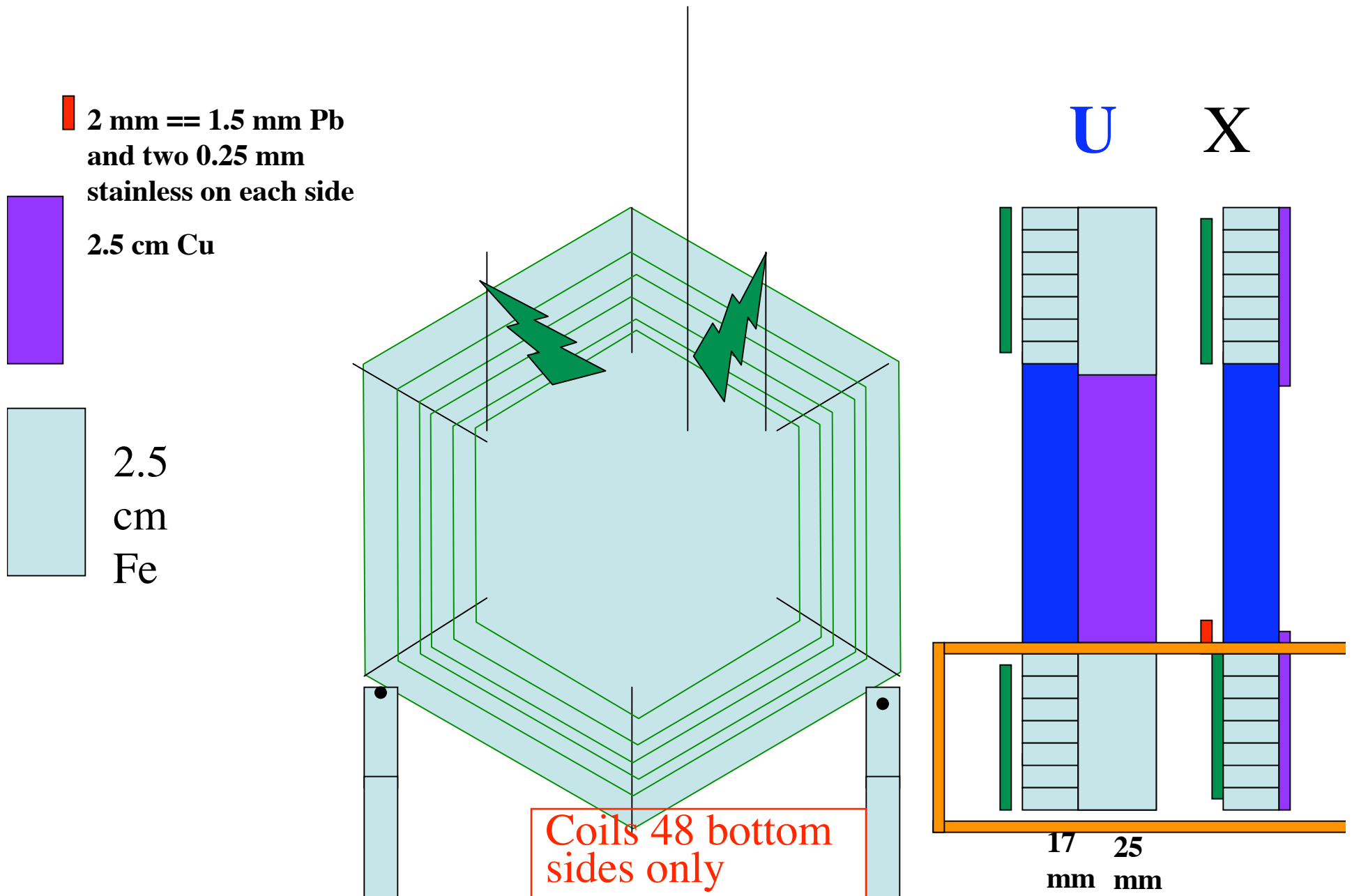
1. Optimize *upstream* Pb EM shower counter and Fe hadron calorimeter to serve a dual function as Pb and Fe targets. Ask Nuclear Targets Subgroup to look into this
2. Optimize exact dimensions and segmentation (current design is pretty close. Ask simulation subgroup to look into this.




Minimize transverse to 4.1 meters to fit within 4.4 m tunnel . Run X-U-X-V-X-U planes at 60 degrees. Use x view to seed the track with 3 hits  
 120 planes of active 1.7 cm target. Total 1.5 m of Scintillator in Z

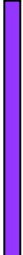


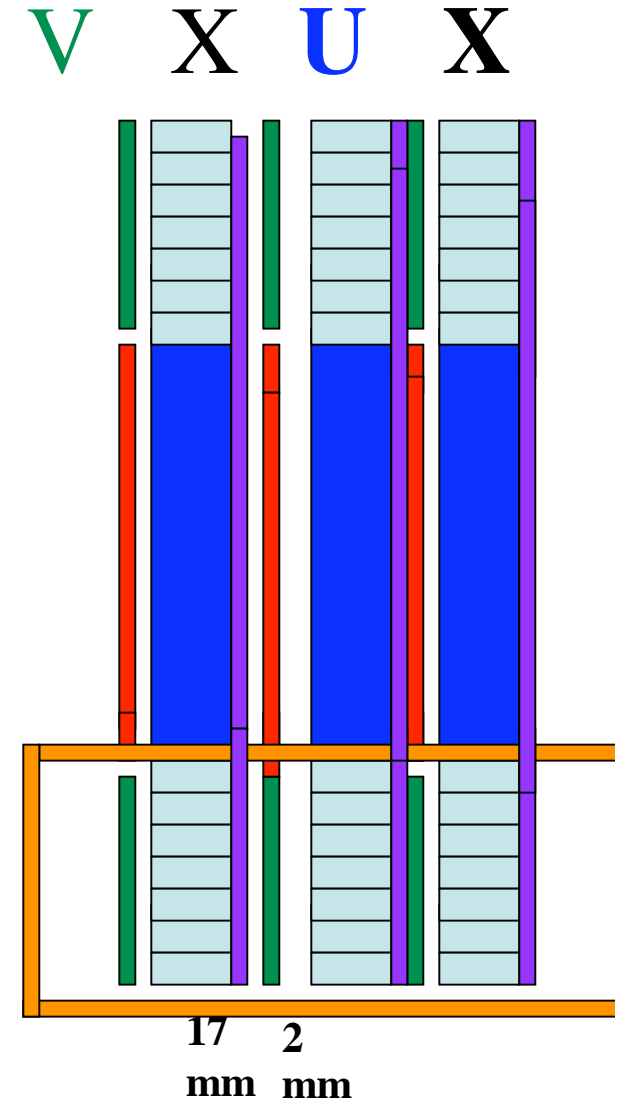
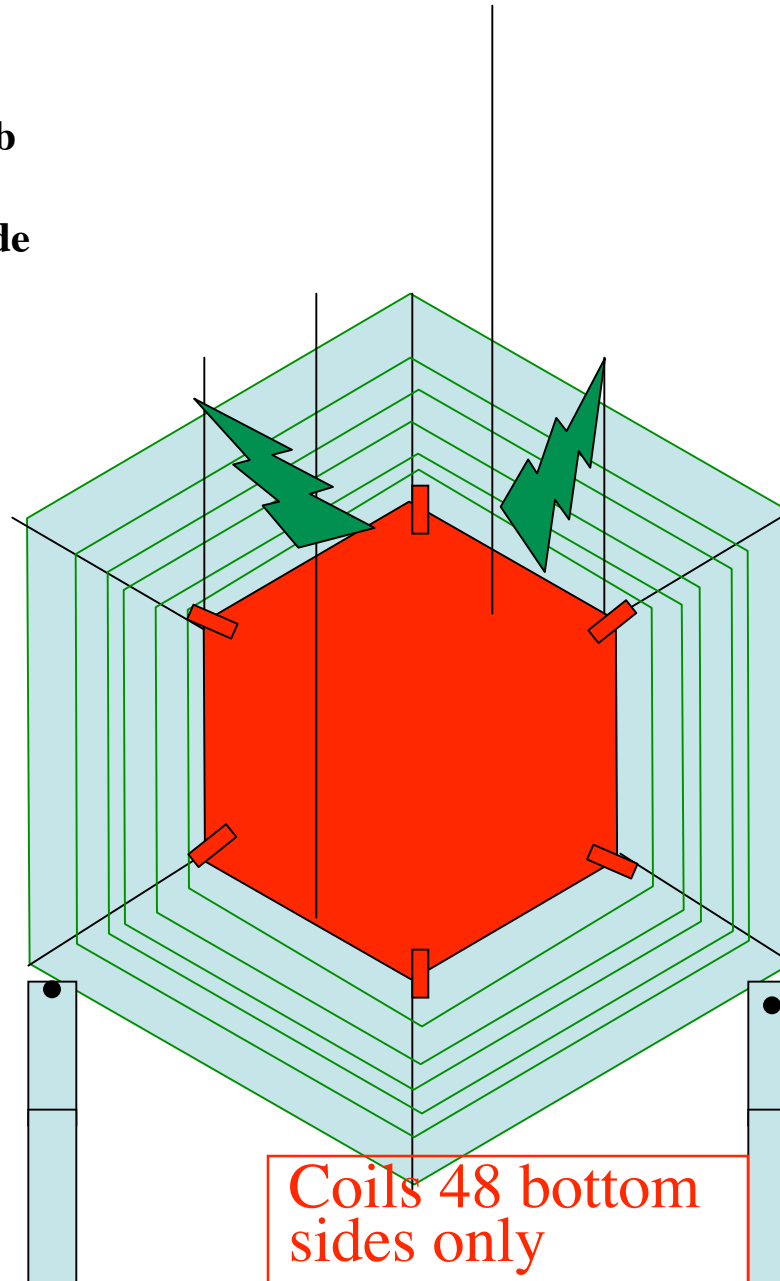
20 planes of HAD calorimeter downstream to fit within 4.4 m tunnel .



20 planes of EM calorimeter downstream to fit within 4.4 m tunnel .

 2 mm == 1.5 mm Pb  
and two 0.25 mm  
stainless on each side

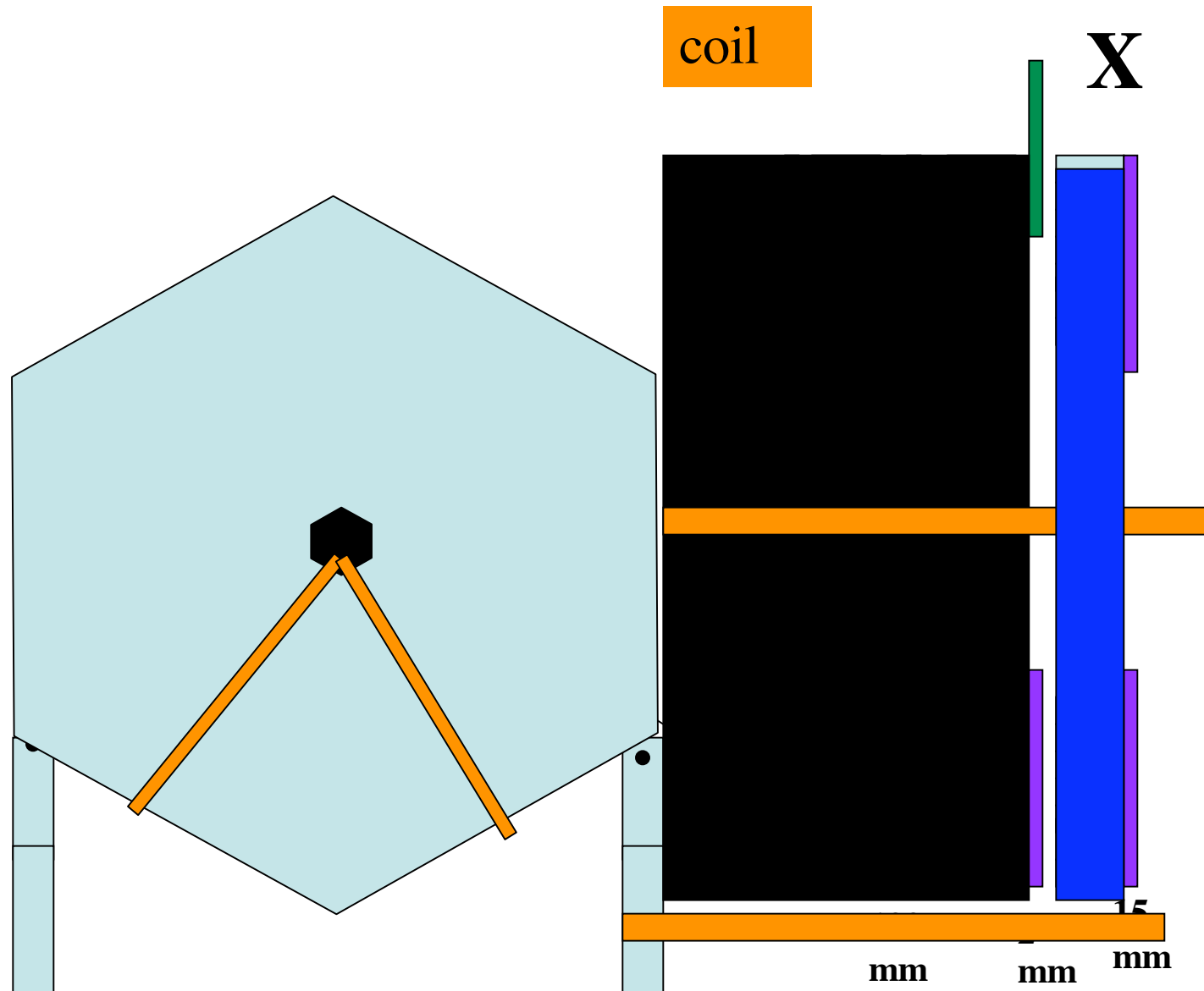
 0.5 mm stainless to  
keep counters in  
place bolted to the  
steel barrel.

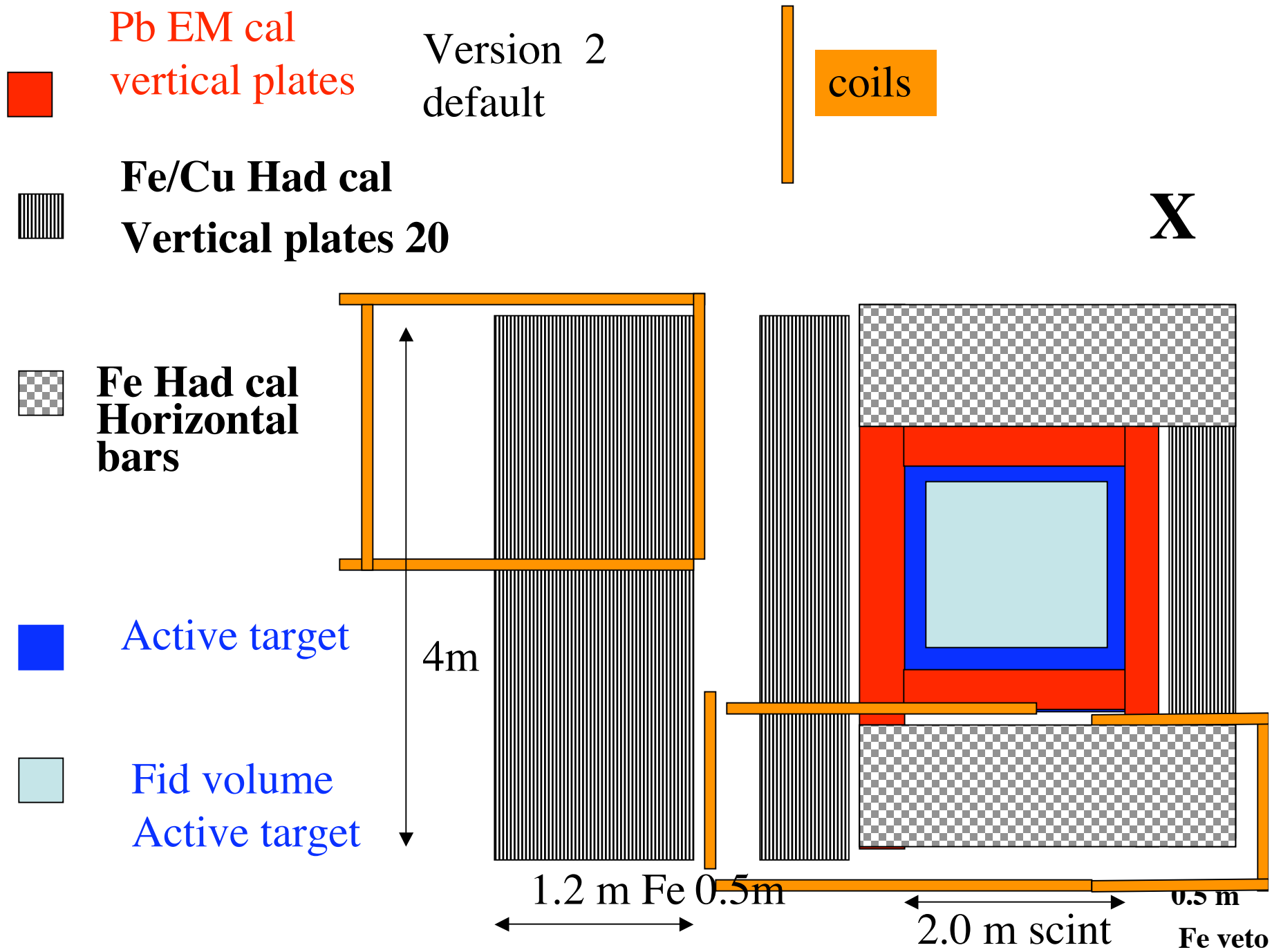


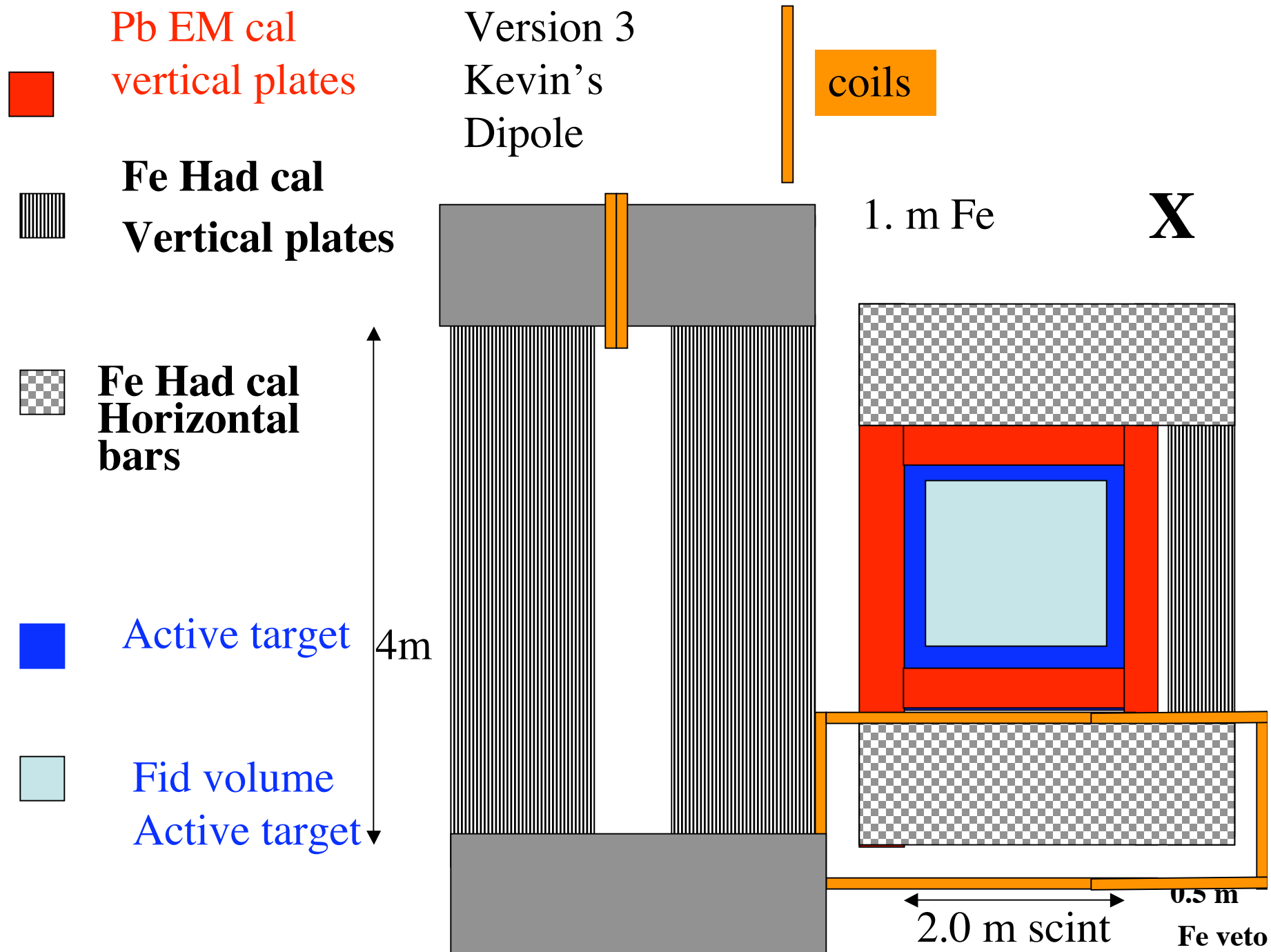
20 planes hadron calorimeter (spaced by 2.5 cm of Cu/FE) downstream  
 followed by 8 planes of muon spectrometer (spaced by 15 cm Fe)

20 cm of  
 Cu/Fe veto  
 upstream

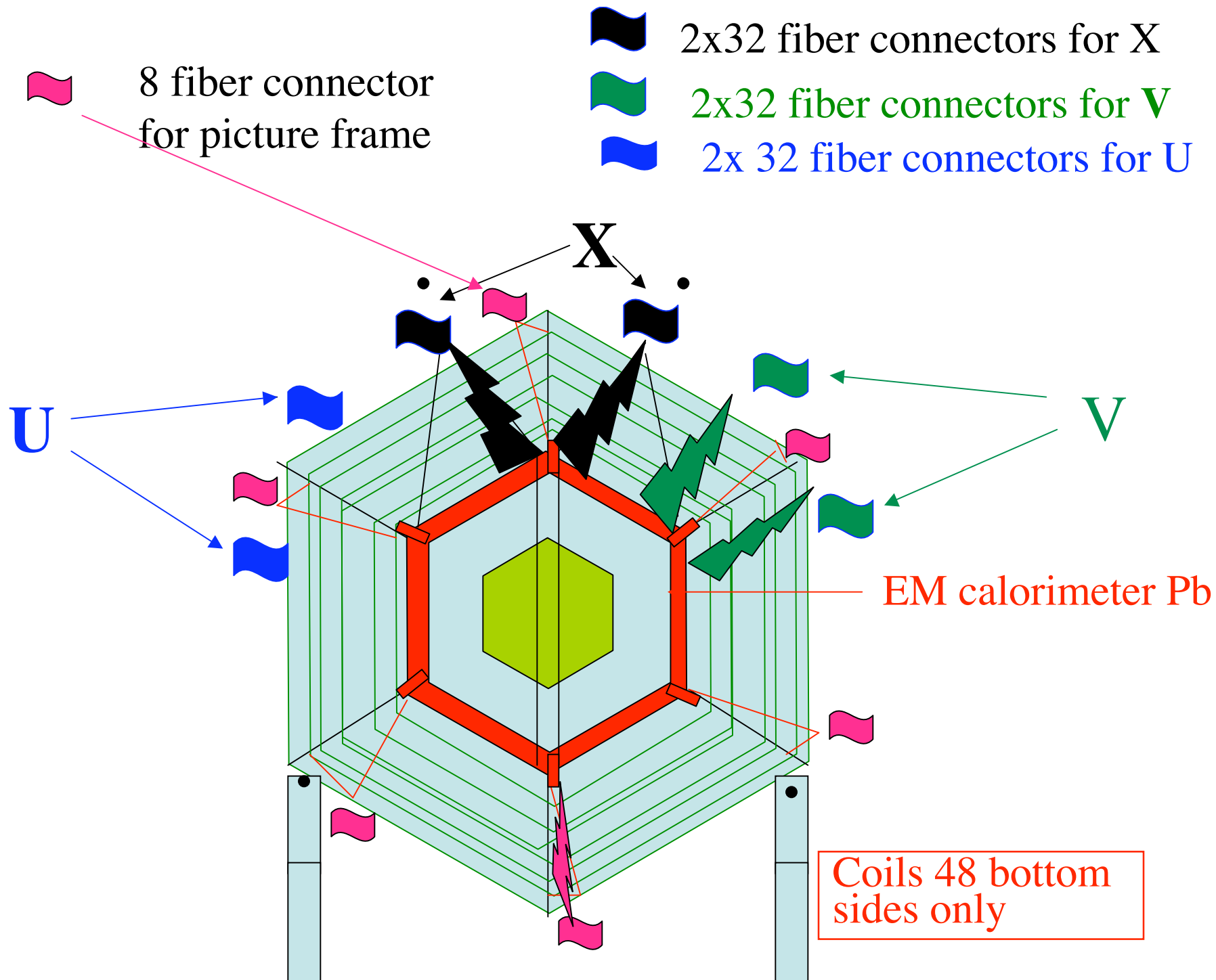
Same as  
 hadron  
 calorimeter  
 but not  
 magnetized











## Target

Basic design - rl of Fe is 1.76 cm and of Pb is 0.56 cm

Active Target = transverse 2.15 meter (1.85m +0.3m) hexagon 64x2 planes 3.35 cm x 1.7 cm thick triangles (the 1.7 cm is to be optimized). Have 120 planes for a total of 2.0 meter of scintillator.  $128 \times 120 = 15,360$  active target channels.). All scintillator 1.85m x1.85m.

Side EM calorimeter Between planes, the outer 0.3 m of active target has washer of 2 mm thickness consisting of 1.5 mm pb (0.27 rl) +0.25x2= 0.5 mm stainless on both sides (total 1 mm of Fe or 0.06 rl. For a total of 0.33 rl. Since it is in the active target, it has X U X V readout. Therefore, inner 1.85 m is fully active and outer 0.3 cm is fully active except for photons. Readout for this is the same as active target, so there are no additional channels

0.94 m Side Hadron Cal/Muon ID. Magnetized steel /of Outer consisting of 2 5 cm Fe plates followed by 6 - 10 cm Fe plates, 8x2 (3. cm 1.7 cm right angle triangle scintillator) for a total thickness of  $70 + 8 \times 3 = 94$  cm with a 2.5 cm steel bars all around for shielding the last counter from background. Total number of channels. Is  $6 \times 8 \times 2 = 96$  - So have  $96 \times 100 = 9600$  side readout channels. (each plane is  $128 + 96 = 224$  channels

## Downstream

Basic design - rl of Fe is 1.76 cm and of Pb is 0.56 cm

Downstream EM calorimeter 20 planes same as a standard plane, except for the fact that Pb absorber now covers the entire inner 2.15 meters. Same as in the target magnetizes the outside steel frame

Downstream Hadron Calorimeter/Muon absorber 20 planes same as downstream EM calorimeter, except for the fact that Pb absorbers are now replaced by 2.5 cm plates of Fe 4 m wide with a hole in the middle for another coil. If we do not have MINOS magnet downstream, then put another 10 planes of 15 cm plates.

Upstream Veto: same as downstream Downstream EM+ Hadron

Calorimeter/Muon absorber except for it being made of 8 Pb+ 4 Fe/Cu plane

Needs to be optimized with MC to see how many backwards particles+energy

Total number of channels: 120 target planes  $\times$  224 = 26,880

Downstream EM calorimeter: 20  $\times$  224 = 4480

Downstream Hadron calorimeter = 20  $\times$  N (=400 cm  $\times$  3/3.35 = 240)

Upstream EM veto = 10 $\times$ 224 plus Upstream Fe Veto = 10 $\times$ 224,  
plus downstream toroid 10 $\times$ 224

# Resolutions Expected

SIMPLE FORMULAE FOR LIGHT YIELD CONSIDERATIONS IN THE DESIGN OF SCINTILLATOR FE AND SCINTILLATOR PB SAMPLING CALORIMETERS.

By Arie Bodek, Priscilla Auchincloss (Rochester U.). UR-1385

Published in Nucl.Instrum.Meth.A357:292-295,1995

On Web as [http://doc.cern.ch/tmp/convert\\_SCAN-9502273.pdf](http://doc.cern.ch/tmp/convert_SCAN-9502273.pdf)

For Resolution of EM calorimeters (with account made for thick scintillator) see: On the energy resolution of electromagnetic sampling calorimeters By J. Del Peso E. Ros Published in Nucl.Instrum.Meth.A276:456-467,1989

**Better formulae for Resolutions:** Note that the EM, Hadron energy resolutions for this detector can be parametrized as the following formulae: EM resolution (from Del Paso et al below) is:

$$\text{Sigma/E EM in percent} = 3.46\% \cdot (\text{t-absorber in rl})^{0.67} / (\text{t-scintillator in rl})^{0.29}$$

Combining information in the articles of Bodek and Auchincloss and Del Paso

$$\text{Sigma/E HAD in percent} = 87\% \cdot (\text{t-absorber in cm}/10 \text{ cm})^{0.67} / (\text{t-scintillator in mm}/25 \text{ mm})^{0.29}$$

**EM calorimeter** part has resolution of  $[4\%/\text{Sqrt}(E_{em})]/\cos\theta$  for 1.5 mm plate Pb and 1.5 cm scintillator.

**Hadron Calorimeter** has resolution of  $[64\%/\text{Sqrt}(E_{had})]/\cos\theta$  for 5 cm Fe sampling and 1.5 cm thick. For normal incidence to the plates  $\cos\theta=1$

Putting into the formula:  $\cos\theta=0.7$  for photons and hadrons at 45 degrees to the planes of the samples one gets : EM calorimeter part has resolution of  $4.5\%/\text{Sqrt}(E_{em})$  for 1.5 mm plate Pb (with 45 degrees incidence) and Hadron Calorimeter for 5 cm sampling has resolution of  $70\%/\text{Sqrt}(E_{had})$  for 45 degree incidence.

3.46	0.670	0.290	SigmaZero	Alpha	Beta	costheta	
5.6	17.6	424	PbX0	FeX0	ScintX0		
1.5	0.5	15	thicknes-mm	thickness-mm	thickness-mm		1
0.26785714	0.02840909	0.03537736	t/X0	t/X0	t/X0		
0.29626623			Pb+Fe				
4.03620092			resolution%	EM			
			times sqrt(E)				
87	0.67	0.29	SigmaZero	Alpha	Beta		
	10	25		Fe	Scint		
	5	15		thickness cm	thickness mm		
	0.5	0.6		tfe/10	tscint/25		
0.5			Fe/10cm				
63.4111009			resolution%	Had			
			times sqrt(E)				



# Resolutions Expected

## Downstream

Hadron calorimeter 5 cm plates with 1.5 cm scintillator. 50 cm total followed by 10 15 cm plates for containment, Total 2 meters of Fe.

Hadron energy resolution of 5 cm section:  $[6\%/\sqrt{E_{had}}]/\cos\theta$

EM calorimeter 20 1/3 rl plates, total 6 rl. Followed by the hadron calorimeter with 5 cm/1.76 = 2.8 rl sampling for containment.

$[4\%/\sqrt{E_{em}}]/\cos\theta$  for 1.5 mm plate Pb and 1.5 cm scintillator.

Side EM planes in same direction as downstream EM so  $4\%/\sqrt{E_{em}}]/\cos\theta$ . Total thickness is 6 rl/cos $\theta$

Side Had has 10 cm sampling so resolution is  $0.87 / \sqrt{E_{had} \sin\theta}$  unless make plates thinner.

### Case of magnetized Steel MINERVA

B-H Curve for steel can be found at [http://www-fmi.fnal.gov/fmiinternal/MI\\_Notes\\_Pages/MI-0127.pdf](http://www-fmi.fnal.gov/fmiinternal/MI_Notes_Pages/MI-0127.pdf) which has been backed up to <http://www.pas.rochester.edu/~bodek/minerva/MI-0127.pdf>

Table 3 page 12 for Armco steel show that for H=10, B=10 Kgauss (B=1 T, or  $\mu=1000$ ). Pretty much around 1000 for lower H. However to get to saturated iron is hard. For H=30, B=15 and for H=60 B=20.5. So need a factor of 6 more current to go from B=10 Kgauss to B=20 Kgauss (below H=10 it is linear). Scaling from CCFR, which has B=1.6 T and L=4.8 meter and resolution of 10%. One gets momentum resolution (which will only be used for sign) of

$$\text{Sigma} = (16\% / B(\text{Tesla}) * \text{Sqrt}[4.8/L(\text{meters})]) \quad \text{Pt kick} = 2.4 \text{ GeV}/c * (B/1.6 \text{ T}) * (L \text{ meter}/4.8\text{m})$$

so for 1.2 iron at 1 T we get sigma of 16% times 2 or 32%. (PT KICK OF 0.44 GeV)

Factor of 2 Better if we use 2 T (see below) which requires factor of 10 more current Energy resolution from range is just how well you can determine range (the more scintillator sampling, the better range is determined).

### What kind of current do we need.

Lab E has 4 coils. 12 turns 1200 amp each. total NI=48x1200 Amp Get 1.9 T at 1 foot and 1.55 T at the edge. 2.4 GeV Pt kick. However, it does not have quality magnet iron steel.

For a square rod going around Minerva of  $L=3.5 \times 4 = 14$  meter so total path of magnetic field is 14 meters (most outer Design, inner path is  $L=3.5 \times 2.15 = 7.5$  meter

$$H = 4 * \pi * (10^{-3}) N I / L \text{ m} \quad \text{in Orested}$$

Need to get H above 10, so running with 48 coils at between 300 and 500 Amps gives B=12 to 14 Kgauss (see spreadsheet).

1.00	1.00	1.00	1.00
1.01	1.01	1.01	1.01
1.02	1.02	1.02	1.02
1.03	1.03	1.03	1.03
1.04	1.04	1.04	1.04
1.05	1.05	1.05	1.05
1.06	1.06	1.06	1.06
1.07	1.07	1.07	1.07
1.08	1.08	1.08	1.08
1.09	1.09	1.09	1.09
1.10	1.10	1.10	1.10
1.11	1.11	1.11	1.11
1.12	1.12	1.12	1.12
1.13	1.13	1.13	1.13
1.14	1.14	1.14	1.14
1.15	1.15	1.15	1.15
1.16	1.16	1.16	1.16
1.17	1.17	1.17	1.17
1.18	1.18	1.18	1.18
1.19	1.19	1.19	1.19
1.20	1.20	1.20	1.20
1.21	1.21	1.21	1.21
1.22	1.22	1.22	1.22
1.23	1.23	1.23	1.23
1.24	1.24	1.24	1.24
1.25	1.25	1.25	1.25
1.26	1.26	1.26	1.26
1.27	1.27	1.27	1.27
1.28	1.28	1.28	1.28
1.29	1.29	1.29	1.29
1.30	1.30	1.30	1.30
1.31	1.31	1.31	1.31
1.32	1.32	1.32	1.32
1.33	1.33	1.33	1.33
1.34	1.34	1.34	1.34
1.35	1.35	1.35	1.35
1.36	1.36	1.36	1.36
1.37	1.37	1.37	1.37
1.38	1.38	1.38	1.38
1.39	1.39	1.39	1.39
1.40	1.40	1.40	1.40
1.41	1.41	1.41	1.41
1.42	1.42	1.42	1.42
1.43	1.43	1.43	1.43
1.44	1.44	1.44	1.44
1.45	1.45	1.45	1.45
1.46	1.46	1.46	1.46
1.47	1.47	1.47	1.47
1.48	1.48	1.48	1.48
1.49	1.49	1.49	1.49
1.50	1.50	1.50	1.50
1.51	1.51	1.51	1.51
1.52	1.52	1.52	1.52
1.53	1.53	1.53	1.53
1.54	1.54	1.54	1.54
1.55	1.55	1.55	1.55
1.56	1.56	1.56	1.56
1.57	1.57	1.57	1.57
1.58	1.58	1.58	1.58
1.59	1.59	1.59	1.59
1.60	1.60	1.60	1.60
1.61	1.61	1.61	1.61
1.62	1.62	1.62	1.62
1.63	1.63	1.63	1.63
1.64	1.64	1.64	1.64
1.65	1.65	1.65	1.65
1.66	1.66	1.66	1.66
1.67	1.67	1.67	1.67
1.68	1.68	1.68	1.68
1.69	1.69	1.69	1.69
1.70	1.70	1.70	1.70
1.71	1.71	1.71	1.71
1.72	1.72	1.72	1.72
1.73	1.73	1.73	1.73
1.74	1.74	1.74	1.74
1.75	1.75	1.75	1.75
1.76	1.76	1.76	1.76
1.77	1.77	1.77	1.77
1.78	1.78	1.78	1.78
1.79	1.79	1.79	1.79
1.80	1.80	1.80	1.80
1.81	1.81	1.81	1.81
1.82	1.82	1.82	1.82
1.83	1.83	1.83	1.83
1.84	1.84	1.84	1.84
1.85	1.85	1.85	1.85
1.86	1.86	1.86	1.86
1.87	1.87	1.87	1.87
1.88	1.88	1.88	1.88
1.89	1.89	1.89	1.89
1.90	1.90	1.90	1.90
1.91	1.91	1.91	1.91
1.92	1.92	1.92	1.92
1.93	1.93	1.93	1.93
1.94	1.94	1.94	1.94
1.95	1.95	1.95	1.95
1.96	1.96	1.96	1.96
1.97	1.97	1.97	1.97
1.98	1.98	1.98	1.98
1.99	1.99	1.99	1.99
2.00	2.00	2.00	2.00

Calculate on  
next slides  
for 2.15 and  
for 4 meter  
long bars  
what is H  
and B for  
several coil  
currents with  
48 turns.

Get muon energy from both range and bend (sign) at low energies and only from bend at higher energies . So for on axis need muon MINOS downstream toroid to get resolutions better than 17%. Downstream we have 2m Fe (or 3 GeV range at zero degrees), side we have 0.7 GeV Fe, or 1 GeV range at 90 degrees.

300	N	48	Res with 0.70 m Fe			kick	kick	kick
			0.7			90	45	30
			angle					
H	B		90	45	30	Pt		
21	13.6		0.31	0.26	0.22	0.30	0.42	0.60
11	10.6		0.40	0.33	0.28	0.23	0.28	0.46
500	N	48	In forward direction we have					Armco Steel
			2 m or a factor of 1.6 better					need 500
			resolution (about 17% resol)					amps
H	B							
35	15.6		0.27	0.23	0.19	0.34	0.41	0.68
19	13.1		0.32	0.27	0.23	0.29	0.34	0.57
150	N	48						
H	B							
11	10.6		0.40	0.33	0.28	0.23	0.28	0.46
8	8.9		0.47	0.40	0.33	0.19	0.23	0.39

At any angle, the Quasielastic muon has the highest possible energy for particles at that angle for a fixed  $E_{\text{zero}}$ .

### scintillator

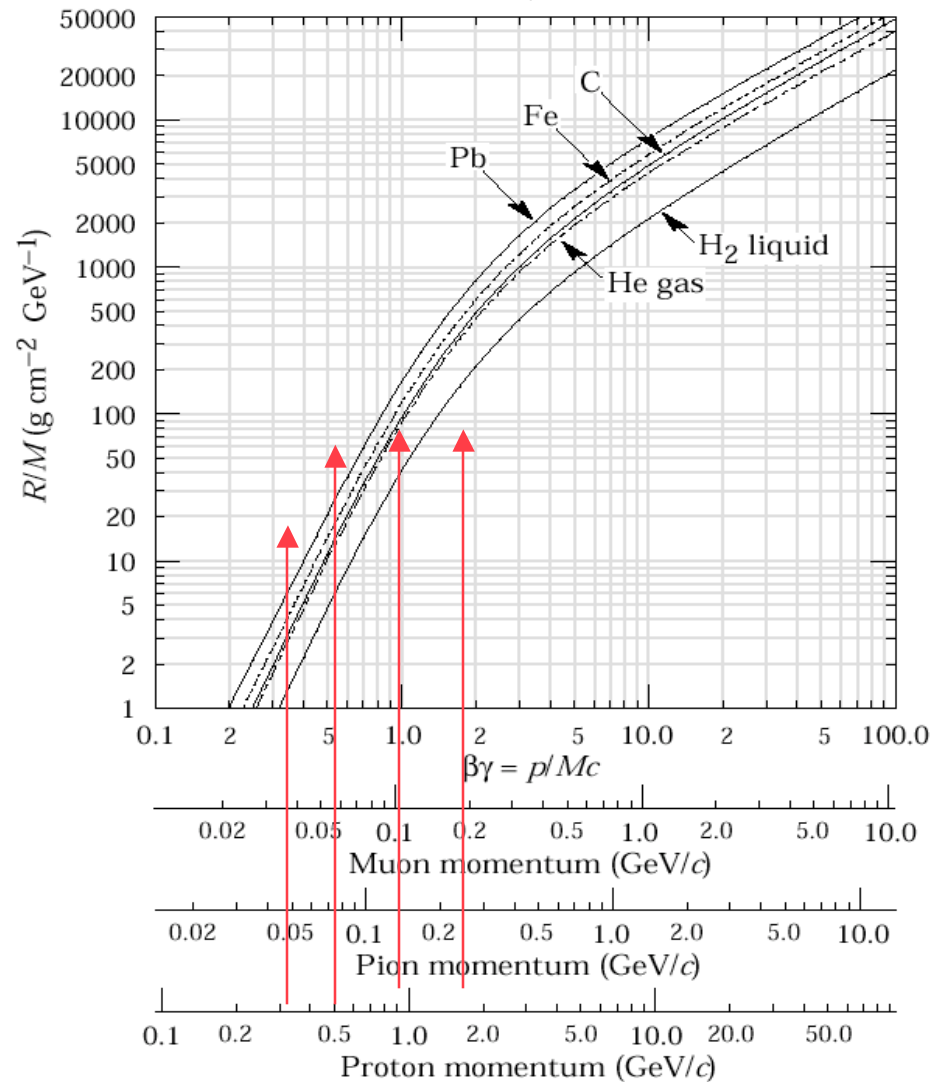
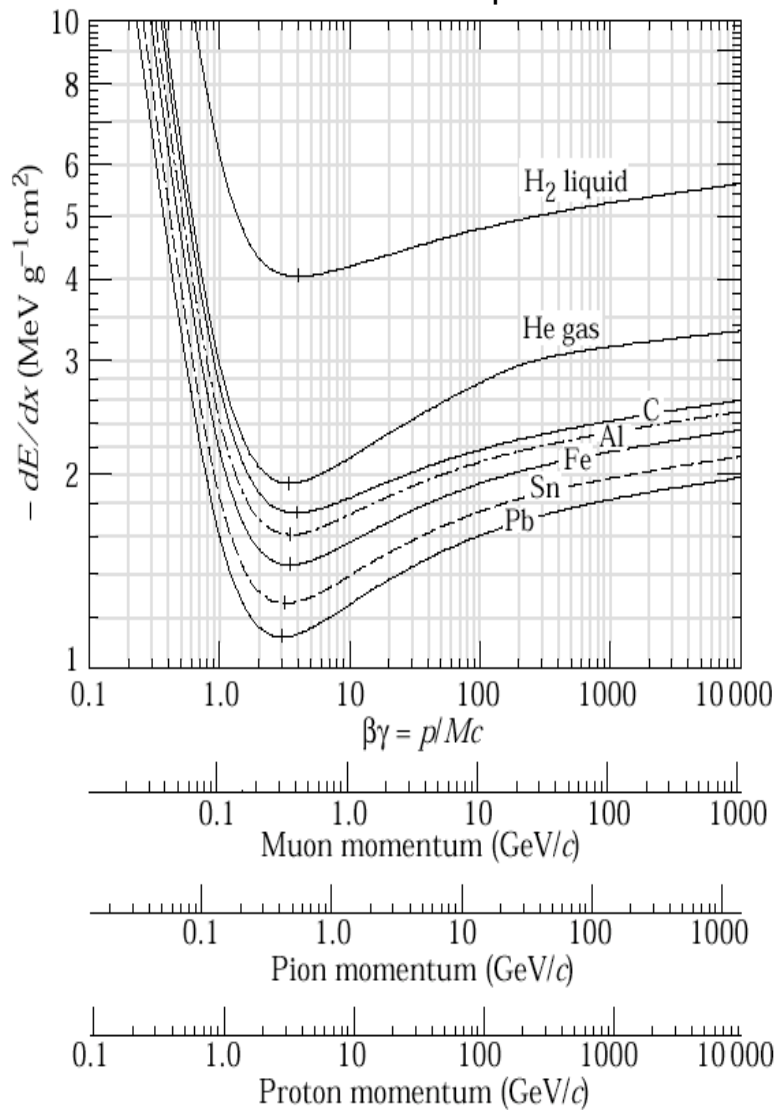
Theta	E'	range m	transverse	Q2
3 Gev	Theta	E' range m	PT of muon	Q2
	0	3	14.3	0
	15	2.71	12.9	0.7
	30	2.10	10.0	1.1
	45	1.55	7.4	1.1
	60	1.15	5.5	1.0
	90	0.71	3.4	0.7
	135	0.46	2.2	0.3
	180	0.41	1.9	0.0
10 Gev				
	0	10.00	47.7	0.0
	15	7.34	35.0	1.9
	30	4.12	19.6	2.1
	45	2.43	11.6	1.7
	60	1.58	7.5	1.4
	90	0.86	4.1	0.9
	135	0.52	2.5	0.4
	180	0.45	2.1	0.0

For muons at 90 degrees, the total range from the edge of the fiducial volume (1m x 1m) includes the 42.5 cm of active target and the 30 cm picture-frame electromagnetic calorimeter and picture frame range detector (including 70 cm of Fe and 12 cm scintillator). Ignoring the Pb, this corresponds to a  $42.5 \text{ cm} + 30 \text{ cm} + 12 \text{ cm} = 85 \text{ cm}$  of scintillator and 70 cm of iron. For muons at 90 degrees this corresponds to a range of  $250 \text{ MeV} + 12 (\text{MeV/cm}) \times 70 = 1090 \text{ MeV}$  which is sufficient to range out all particles at 90 degrees for  $E_0$  of 3 GeV (maximum  $E'$  at 90 degrees of 710 MeV). Since the iron is magnetized, the particles bend forward so the effective absorption of the range is higher than 1.1 GeV

For muons at 45 degrees, the range of the picture-frame side absorber is increased by a factor of 1.414 (to 1.54 GeV), which ranges out a 45 degree quasielastic muon ( $E' = 1.52 \text{ GeV}$ ) for  $E_0$  of 3 GeV. Therefore, even for neutrinos produced at the edge of the 1m x 1m active fiducial area, all quasielastic muons are contained. The fact that the muons bend forward adds another margin of safety.



Back of envelope estimates - needs to be done more quantitatively



For  $Q^2=0.110$  GeV<sup>2</sup>,  $q_3=P=0.330$  GeV

Proton kinetic energy =  $P^2/2M = 55$  MeV

Range about 5 cm - Note nuclear binding about 30 MeV

0.5 GeV P = 15 cm of scintillator = 120 MeV energy

Versus 1 mip = 2 MeV/cm.

Get 60 mips

Copy of Sept 4. 2003 Email

I have put Hexagonal design draft which can be put into on-axis or off-axis tunnel. File is at <http://www.pas.rochester.edu/~bodek/> directory minerva file name hexagon-design.ppt

Concept is that EM calorimeter is like Tanakos idea of washers, but using Stainless steel clad Pb Plates. So it takes almost no room in Z. The hadron/muon calorimeter is using the picture frame design, because any other design does not give much Bx $\Delta L$  (formulae for resolutions are in the PPT file).

This design can be put as a default, and parameters varied and optimized. I have formulae that will calculate any muon resolution versus angle in the PPT file and hadron energy resolution and EM energy resolution below (and attached spreadsheet)

Please look at the design on this Web page. I will try to work on the file and update it. The exact resolutions are given in this Email (and attached spreadsheet) for EM and Hardron. I drew up a hexagon design in detail I also drew to scale.

Need about 27K channels. Also, as you will see, the detector is kind of square, so side detector only looks at particles greater than 45 degrees. We expect large angle and backward particles. I suggest that you look at 3 GeV neutrinos to see where particles go