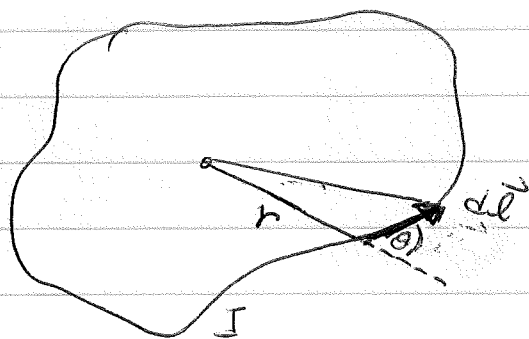


$$\vec{B} = \frac{3(\vec{m} \cdot \hat{r})\hat{r} - \vec{m}}{r^3}$$

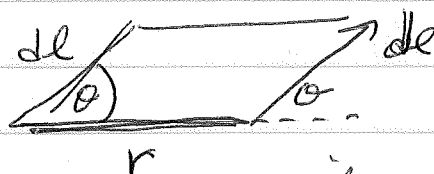
same form as $\vec{E}$ from electric dipole $\vec{p}$

For a current loop in a plane (any shape loop provided it is flat)

$$\vec{m} = \frac{1}{2c} \int d^3r \vec{r} \times \vec{j} = \frac{1}{2c} I \oint \vec{r} \times d\vec{l}$$



$$\begin{aligned} \text{area of triangle is } & \frac{1}{2} r dl \sin \theta \\ & = \frac{1}{2} |\vec{r} \times d\vec{l}| \end{aligned}$$



$$\text{area of } \text{parallelogram} \text{ is } r dl \sin \theta$$

$$\Rightarrow \vec{m} = \frac{1}{2c} I (\text{area}) \hat{n}$$

$\uparrow$
area of loop

$\nwarrow$ outward normal

(direction given by right hand rule with respect to direction of current)

magnetic dipole moment $\vec{m}$ is independent of location of origin.

$$\vec{r}' = \vec{r} + \vec{d} \quad \text{new coord}$$

$$\begin{aligned} \vec{m}' &= \frac{1}{2c} \int d^3 r' (\vec{r}' \times \vec{j}) = \frac{1}{2c} \int d^3 r (\vec{r} + \vec{d}) \times \vec{j} \\ &= \frac{1}{2c} \int d^3 r \vec{r} \times \vec{j} + \frac{1}{2c} \vec{d} \times \left[\int d^3 r \vec{j} \right] \end{aligned}$$

$$\vec{m}' = \vec{m} + 0 \quad \text{as } \int d^3 r \vec{j} = 0$$

for planar loop $\vec{m} = \frac{Ia}{c} \hat{n}$ where $a = \text{area}$
 $\hat{n} = \text{outward normal}$

can also apply to get $\vec{m}$ for piecewise planar loops

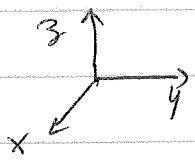


Diagram showing a square loop in the xy-plane, which is the superposition of two smaller square loops, labeled ① and ②. Loop ① is in the upper half (positive y) and loop ② is in the lower half (negative y). Both loops have current flowing in the same direction (counter-clockwise when viewed from above).

$$\vec{m} = \vec{m}_1 + \vec{m}_2$$

$$\vec{m}_1 = \frac{Ia_1}{c} \hat{x}$$

$$\vec{m}_2 = \frac{Ia_2}{c} \hat{z}$$

$$\Rightarrow \vec{m} = \frac{I}{c} (a_1 \hat{x} + a_2 \hat{z})$$

Boundary value problems in magnetostatics

Scalar Magnetic Potential

Because of the vector character of the equation

$$-\nabla^2 \vec{A} = \frac{4\pi}{c} \vec{j}$$

and the fact that $\nabla^2 \vec{A}$ only has a convenient representation in Cartesian coordinates, many of the methods we used to solve the scalar $-\nabla^2 \phi = 4\pi \rho$ don't work so well for magnetostatics.

However, in situations where the current $\vec{j}$ is confined to certain surfaces, we can make things much closer to the electrostatic case by using the trick of the scalar magnetic potential ϕ_M .

In regions where $\vec{j} = 0$, i.e. not on the certain surfaces, we have $\vec{\nabla} \cdot \vec{B} = 0$ and $\vec{\nabla} \times \vec{B} = 0$. Since $\vec{\nabla} \times \vec{B} = 0$ in these regions we can define a scalar potential ϕ_M such that

$$\vec{B} = -\vec{\nabla} \phi_M$$

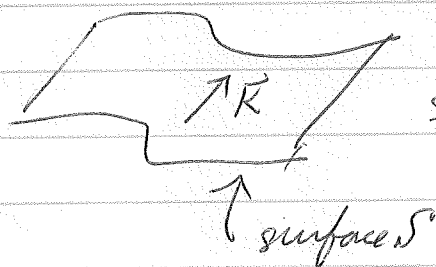
and then

$$\vec{\nabla} \cdot \vec{B} = -\nabla^2 \phi_M = 0$$

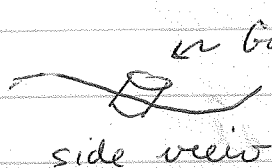
We can solve for ϕ_M as in electrostatics, and match solutions by applying appropriate boundary conditions on the current carrying surfaces.

Boundary Conditions at Sheet current

in magnetostatics $\vec{\nabla} \cdot \vec{B} = 0$, $\vec{\nabla} \times \vec{B} = \frac{4\pi}{c} \vec{j}$



surface current $\vec{K}(\vec{r})$ at pt $\vec{r}$
on surface S



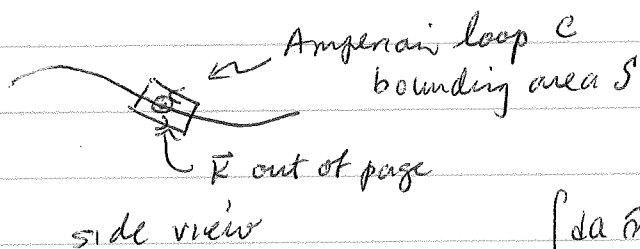
Gaussian pillbox vol V

$$\int_V d^3r \vec{\nabla} \cdot \vec{B} = 0$$

top + bottom area of pill box is da
width of pill box $\rightarrow 0$

$$\Rightarrow \int_V d^3r \vec{\nabla} \cdot \vec{B} = \oint_S da \hat{n} \cdot \vec{B} = da (\vec{B}_{\text{above}} - \vec{B}_{\text{below}}) \cdot \hat{n} = 0$$

normal component of $\vec{B}$ is continuous $(\vec{B}_{\text{above}} - \vec{B}_{\text{below}}) \cdot \hat{n} = 0$



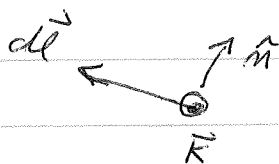
Amperian loop C
bounding area S

$\vec{K}$ out of page

side view

$$\oint_S da \hat{n} \cdot (\vec{\nabla} \times \vec{B}) = \oint_C \vec{B} \cdot d\vec{\ell} = \frac{4\pi}{c} I_{\text{enclosed}}$$

let width of loop $\rightarrow 0$, top + bottom sides $d\vec{\ell}$



$\hat{n}$ is outward normal

$$(\vec{B}_{\text{above}} - \vec{B}_{\text{below}}) \cdot d\vec{\ell} = \frac{4\pi}{c} (\hat{n} \times d\vec{\ell}) \cdot \vec{K}$$

$$= \frac{4\pi}{c} (\vec{K} \times \hat{n}) \cdot d\vec{\ell}$$

tangential component of $\vec{B}$ has

discontinuous jump $\frac{4\pi}{c} \vec{K} \times \hat{n}$

Combine both results into

$$\vec{B}_{\text{above}} - \vec{B}_{\text{below}} = \frac{4\pi}{c} \vec{K} \times \hat{n}$$

magnetic analog of $\vec{E}_{\text{above}} - \vec{E}_{\text{below}} = 4\pi\sigma \hat{n}$

In terms of magnetic ^{scalar} ~~vector~~ potential Φ_M

$$-\vec{\nabla}\Phi_{M\text{above}} + \vec{\nabla}\Phi_{M\text{below}} = \frac{4\pi}{c} \vec{K} \times \hat{n}$$

Note: Φ_M is a calculational tool only

it does not have any direct physical significance as does the electrostatic ϕ .

Electrostatic ϕ is related to work done

moving a charge $W_{12} = q[\phi(r_2) - \phi(r_1)]$

nothing similar for Φ_M .

(in fact ~~magnetostatic~~ magnetic forces do no work!

$$\vec{F} = q \vec{v} \times \vec{B}$$

$$\Rightarrow \vec{F} \cdot \vec{v} = \frac{dW}{dt} = 0)$$

Note:

Φ_M is not necessarily continuous at surface current
Cannot do similar to electrostatics and use

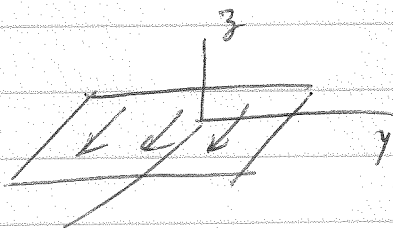
$$\Phi_M(r_{\text{above}}) - \Phi_M(r_{\text{below}}) = - \int_{r_{\text{below}}}^{r_{\text{above}}} \vec{B} \cdot d\vec{l}$$

Since Φ_M is not defined on the current sheet itself, separating "above" from "below".

example

Flat infinite plane at $z=0$ with surface current

$$\vec{K} = K \hat{x}$$



x

$$z \geq 0, \nabla^2 \phi_M^> = 0 \Rightarrow \phi_M^> = a^> - b_x^> x - b_y^> y - b_z^> z$$

$$z < 0, \nabla^2 \phi_M^< = 0 \Rightarrow \phi_M^< = a^< - b_x^< x - b_y^< y - b_z^< z$$

$$z \geq 0, \vec{B}^> = -\vec{\nabla} \phi_M^> = b_x^> \hat{x} + b_y^> \hat{y} + b_z^> \hat{z}$$

$$z < 0, \vec{B}^< = -\vec{\nabla} \phi_M^< = b_x^< \hat{x} + b_y^< \hat{y} + b_z^< \hat{z}$$

$$\begin{aligned} \text{at } z=0 \quad \vec{B}^> - \vec{B}^< &= (b_x^> - b_x^<) \hat{x} + (b_y^> - b_y^<) \hat{y} + (b_z^> - b_z^<) \hat{z} \\ &= \frac{4\pi K}{c} \hat{x} \times \hat{m} = \frac{4\pi K}{c} (\hat{x} \times \hat{z}) = -\frac{4\pi K}{c} \hat{y} \end{aligned}$$

$$\Rightarrow b_x^> = b_x^< \equiv b_{x0}, \quad b_z^> = b_z^< \equiv b_{z0}, \quad b_y^> - b_y^< = -\frac{4\pi K}{c}$$

$$\text{define } \left. \begin{aligned} b_y^> &= b_{y0} + \delta b_y \\ b_y^< &= b_{y0} - \delta b_y \end{aligned} \right\} \delta b_y = -\frac{2\pi K}{c}$$

$$\Rightarrow \vec{B}^> = \vec{B}_0 - \frac{2\pi K}{c} \hat{y}$$

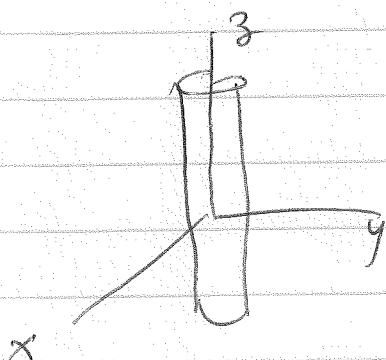
$$\vec{B}^< = \vec{B}_0 + \frac{2\pi K}{c} \hat{y}$$

$$\vec{B}_0 = b_{x0} \hat{x} + b_{y0} \hat{y} + b_{z0} \hat{z}$$

if $\vec{K}$ is the only source of magnetic field then $\vec{B}_0 = 0$

$$\vec{B} = \begin{cases} -\frac{2\pi K}{c} \hat{y} & z > 0 \\ \frac{2\pi K}{c} \hat{y} & z < 0 \end{cases}$$

example current carrying infinite cylinder radius R



- (i) $\vec{K} = K \hat{z}$ wire with surface current
 (ii) $\vec{K} = K \hat{\phi}$ solenoid

(2) $\vec{K} = K \hat{z}$

$2\pi R K = I$ total current
 ← "guess" + show it is correct

$$\begin{aligned} r > R & \quad \boxed{\phi_M = -\frac{4\pi R K}{c} \phi} \\ r < R & \quad \phi_M = 0 \end{aligned}$$

magnetic scalar potential $\nabla^2 \phi_M = 0$

$$\begin{aligned} r > R & \quad \vec{B} = -\vec{\nabla} \phi_M = -\frac{1}{r} \frac{\partial \phi_M}{\partial \phi} \hat{\phi} = \frac{4\pi R K}{c r} \hat{\phi} = \boxed{\frac{2I}{c r} \hat{\phi}} \\ r < R & \quad \vec{B} = 0 \end{aligned}$$

← familiar result from Ampere

$$\vec{B}_{\text{above}} - \vec{B}_{\text{below}} = \frac{2I}{cR} \hat{\phi} = \frac{4\pi K}{c} \frac{R}{R} \hat{\phi} = \frac{4\pi \vec{K}}{c} \times \hat{n}$$

where $\hat{n} = \hat{r}$
 as $\hat{z} \times \hat{r} = \hat{\phi}$

Note: $\phi_M = -\frac{4\pi R K}{c} \phi$ is not single valued!

would not have found this using expansion of separation of coords in polar coords

ϕ_M does not need to be single valued since it has no physical significance, only $\vec{B} = -\vec{\nabla} \phi_M$ is physical

(iii) $\vec{K} = K \hat{\phi}$

$$r > R \quad \phi_M = -B_1 z$$

$$r < R \quad \phi_M = -B_2 z$$

$$r > R \quad \vec{B} = -\vec{\nabla} \phi_M = B_1 \hat{z}$$

$$r < R \quad \vec{B} = -\vec{\nabla} \phi_M = B_2 \hat{z}$$

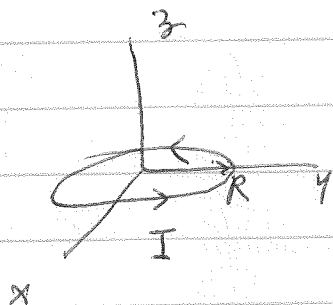
$$\left. \begin{aligned} & \\ & \end{aligned} \right\} \nabla^2 \phi_M = 0$$

$$\begin{aligned}
 \vec{B}_{\text{above}} - \vec{B}_{\text{below}} &= (B_1 - B_2) \hat{z} = \frac{4\pi}{c} \vec{K} \times \hat{n} \\
 &= \frac{4\pi}{c} K (\hat{\phi} \times \hat{r}) \\
 &= -\frac{4\pi K}{c} \hat{z}
 \end{aligned}$$

If current in solenoid is only source of $\vec{B}$ then expect $B_1 = 0$

$$\Rightarrow \boxed{\vec{B}_2 = \frac{4\pi K}{c} \hat{z}} \quad \text{familiar result}$$

example circular current loop in xy plane
radius R



for $r > R$, $\vec{\nabla} \times \vec{B} = 0 \Rightarrow \vec{B} = -\vec{\nabla} \phi_M$
where $\nabla^2 \phi_M = 0$.

Try Legendre polynomial expansion for ϕ_M

$$\phi_M = \sum_{l=0}^{\infty} \frac{B_l}{r^{l+1}} P_l(\cos\theta) \quad (A_l \text{ terms vanish as want } B \rightarrow 0 \text{ as } r \rightarrow \infty)$$

$$\vec{B} = -\vec{\nabla} \phi_M = -\frac{\partial \phi_M}{\partial r} \hat{r} - \frac{1}{r} \frac{\partial \phi_M}{\partial \theta} \hat{\theta}$$

$$= \sum_l \left[\frac{(l+1)B_l}{r^{l+2}} P_l(\cos\theta) \hat{r} - \frac{B_l}{r^{l+2}} \frac{\partial P_l(\cos\theta)}{\partial \theta} \hat{\theta} \right]$$

with $\frac{\partial P_l}{\partial \theta} = \frac{\partial P_l}{\partial x} \frac{\partial x}{\partial \theta} = -\frac{\partial P_l}{\partial x} \sin\theta$ $x = \cos\theta$
 $= -P'_l \sin\theta$

$$\vec{B} = \sum_l \left[\frac{(l+1)B_l}{r^{l+2}} P_l(\cos\theta) \hat{r} + \frac{B_l \sin\theta}{r^{l+2}} P'_l(\cos\theta) \hat{\theta} \right]$$

To determine the B_l we compare with exact solution along $\hat{z}$ axis

$$\vec{B}(z\hat{z}) = \sum_l \frac{(l+1)B_l}{r^{l+2}} \hat{r} = \sum_l \frac{(l+1)B_l}{z^{l+2}} \hat{z}$$

since $P_l(1)=1$, $\sin(0)=0$ and $P'_l(1)$ finite, $\hat{r} = \hat{z}$ when $\theta=0$

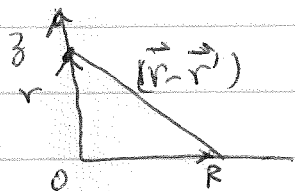
exact solution on $\hat{z}$ axis:

$$\vec{A} = \int \frac{d^3 r'}{c} \frac{\vec{j}(\vec{r}')}{|\vec{r} - \vec{r}'|} \Rightarrow \vec{B}(\vec{r}) = \vec{\nabla} \times \vec{A} = \int \frac{d^3 r'}{c} \vec{\nabla} \times \frac{\vec{j}(\vec{r}')}{|\vec{r} - \vec{r}'|}$$

$$\vec{B} = - \int \frac{d^3 r'}{c} \vec{j}(\vec{r}') \times \vec{\nabla} \left(\frac{1}{|\vec{r} - \vec{r}'|} \right)$$

$$\vec{B} = \int \frac{d^3 r'}{c} \vec{j}(\vec{r}') \times \frac{(\vec{r} - \vec{r}')}{|\vec{r} - \vec{r}'|^3} \quad \text{Biot-Savart Law for magnetostatics}$$

For our loop



$$\vec{B}(z) = \int_0^{2\pi} d\phi \frac{R}{c} I \hat{\phi} \times \frac{[z\hat{z} - R\hat{r}]}{(z^2 + R^2)^{3/2}}$$

polar radial vector

$$\hat{r} \times \hat{\phi} = \hat{z}$$

$$= \int_0^{2\pi} d\phi \frac{R(I R)}{c} \frac{\hat{z}}{(z^2 + R^2)^{3/2}}$$

$\hat{\phi} \times \hat{z}$ term
integrates to zero

$$\boxed{\vec{B}(z) = \frac{2\pi R^2 I}{c} \frac{\hat{z}}{(z^2 + R^2)^{3/2}}}$$

to match Legendre polynomial expansion, do Taylor series expansion of above

$$\vec{B}(z) = \frac{2\pi R^2 I}{c} \frac{\hat{z}}{z^3} \frac{1}{(1 + (\frac{R}{z})^2)^{3/2}} = \frac{2\pi R^2 I}{c} \frac{\hat{z}}{z^3} \left\{ 1 - \frac{3}{2} \left(\frac{R}{z} \right)^2 + \dots \right\}$$

$$= \frac{2\pi R^2 I}{c} \frac{\hat{z}}{z^3} \left\{ \frac{1}{z^3} - \frac{3}{2} \frac{R^2}{z^5} + \dots \right\}$$

$$= \left\{ \frac{B_0}{z^2} + \frac{2B_1}{z^3} + \frac{3B_2}{z^4} + \frac{4B_3}{z^5} + \dots \right\} \hat{z}$$

$$\Rightarrow B_0 = 0, \quad B_1 = \frac{\pi R^2 I}{c}, \quad B_2 = 0, \quad B_3 = -\frac{3\pi R^2 I R^2}{4c}$$

So to order $L=3$

$$\vec{B}(\vec{r}) = \frac{\pi R^2 I}{c} \left\{ \frac{2 P_1(\cos\theta) \hat{r} + \sin\theta P_1'(\cos\theta) \hat{\theta}}{r^3} - \left[\frac{3 R^2 P_3(\cos\theta) \hat{r} + \frac{3}{4} R^2 \sin\theta P_3'(\cos\theta) \hat{\theta}}{r^5} \right] + \dots \right\}$$

$$P_1(x) = x \Rightarrow P_1'(x) = 1$$

$$P_3(x) = \frac{1}{2}(5x^3 - 3x) \Rightarrow P_3'(x) = \frac{1}{2}(15x^2 - 3)$$

$$\vec{B}(\vec{r}) = \frac{\pi R^2 I}{c} \left\{ \frac{2 \cos\theta \hat{r} + \sin\theta \hat{\theta}}{r^3} - \left[\frac{\frac{3}{2} R^2 (5 \cos^3\theta - 3 \cos\theta) \hat{r} + \frac{3}{8} R^2 \sin\theta (15 \cos^2\theta - 3) \hat{\theta}}{r^5} \right] + \dots \right\}$$

$\frac{\pi R^2 I}{c} = m$ is the magnetic dipole moment of the loop

We see that the 1st term is just the magnetic dipole approx. The 2nd term is the magnetic octopole term. Could easily get higher order terms by this method.

Compare our result above to Jackson (5.40)