

Then we get

$$M = \frac{N}{V} = \frac{n(0)}{V} + \frac{g_{3/2}(z)}{\lambda^3}$$

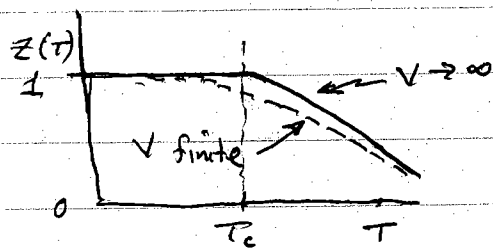
$$M = M_0 + \frac{g_{3/2}(z)}{\lambda^3} \quad \text{where } M_0 = \frac{n(0)}{V} \text{ density of bosons in ground state}$$

For a system with fixed m , at higher T one can always choose z so that $m = \frac{g_{3/2}(z)}{\lambda^3}$ and $M_0 = 0$.

But when $T < T_c$ it is necessary to have $M_0 > 0$.

Using $n(0) = \frac{z}{1-z}$ we can write above as

$$M = \frac{z}{1-z} \frac{1}{V} + \frac{g_{3/2}(z)}{\lambda^3}$$



For $T > T_c$ we will have a solution to the above for some fixed $z < 1$. In thermodynamic limit $V \rightarrow \infty$, the first term will then vanish, i.e. the density of bosons in the ground state vanishes.

As $T \rightarrow T_c$, $z \rightarrow 1$ and ^{as $V \rightarrow \infty$} the first term $\left(\frac{z}{1-z}\right)\left(\frac{1}{V}\right)$ stays finite to give the additional needed density at $T < T_c$:

$$\frac{z}{1-z} \frac{1}{V} = M_0 = m - \frac{g_{3/2}(1)}{\lambda^3}$$

↑ diverges as $z \rightarrow 1$ ↑ vanishes as $V \rightarrow \infty$

T_c defines the Bose-Einstein transition temperature below which the system develops a finite density of particles in the ground state n_0 .

n_0 is also called the condensate density.

The particles in the ground state are called the condensate.

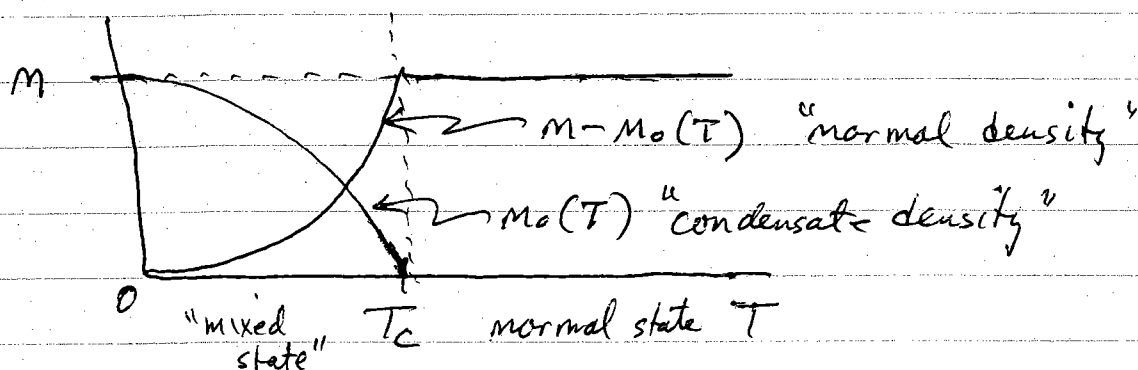
$$\left. \begin{array}{l} z(T) \rightarrow 1 \\ \mu(T) \rightarrow 0 \end{array} \right\} \text{ as } T \rightarrow T_c, \quad \left. \begin{array}{l} z(T) = 1 \\ \mu(T) = 0 \end{array} \right\} \text{ for } T \leq T_c$$

For $T \leq T_c$

$$n_0(T) = n - \frac{g_{3/2}(1)}{\lambda^3} = n - 2.612 \left(\frac{2\pi m k_B T}{h^2} \right)^{3/2}$$

$$n_0(T) = n \left(1 - \left(\frac{T}{T_c} \right)^{3/2} \right)$$

condensate density vanishes continuously as $T \rightarrow T_c$ from below



At $T=0$, all bosons are in condensate

At $T > T_c$, all bosons are in the "normal state"

At $0 < T < T_c$, a macroscopic fraction of bosons are in the condensate, while the remaining fraction are in the normal state — call it the "mixed state"

pressure - separate out ground state from sum as we saw we needed to do in computing N/V

$$\frac{p}{k_B T} = \frac{1}{V} \ln \mathcal{Z} = -\frac{1}{V} \sum_{\vec{k}} \ln (1 - z e^{-\beta \epsilon(\vec{k})})$$

$$\approx -\frac{1}{V} \ln (1-z) - \frac{4\pi}{(2\pi)^3} \int_0^{\infty} dk k^2 \ln (1 - z e^{-\beta \hbar^2 k^2 / 2m})$$

$\uparrow$
 $\vec{k}=0$ ground state

 $\uparrow$
 all other $|\vec{k}| > 0$ states

$$= \frac{1}{V} \ln \left(\frac{1}{1-z} \right) + \frac{g_{5/2}(z)}{\lambda^3} \quad \lambda = \left(\frac{\hbar^2}{2\pi m k_B T} \right)^{1/2}$$

where $g_{5/2}(z) \equiv \frac{1}{\Gamma(5/2)} \int_0^{\infty} dy \frac{y^{3/2}}{z^{-1} e^y - 1}$ as derived when we began our discussion of quantum gases

also recall the number of bosons occupying the ground state is

$$n(0) = \frac{1}{z^{-1} e^{\beta \epsilon(0)} - 1} = \frac{1}{z^{-1} - 1} = \frac{z}{1-z}$$

So $n(0) + 1 = \frac{z}{1-z} + 1 = \frac{1}{1-z}$

$$\frac{p}{k_B T} = \frac{\ln(n(0)+1)}{V} + \frac{g_{5/2}(z)}{\lambda^3}$$

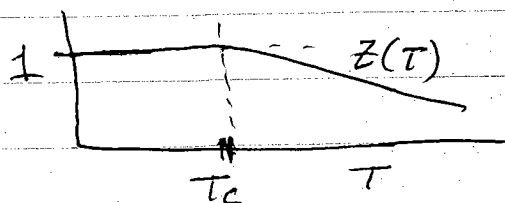
In the thermodynamic limit of $V \rightarrow \infty$, the first term always vanishes as $n(0) \leq N = nV$ and $\lim_{V \rightarrow \infty} \left[\frac{\ln(nV)}{V} \right] = 0$

So the condensate does not contribute to the pressure. This is not surprising as particles in the condensate have $\vec{k}=0$ and hence carry no momentum. In the kinetic theory of gases, one sees that pressure arises from particles with finite momentum $|\vec{p}| > 0$ hitting the walls of the container

$$\text{So } \frac{p}{k_B T} = \frac{g_{5/2}(z)}{\lambda^3} = g_{5/2}(z) \left(\frac{2\pi m k_B T}{h^2} \right)^{3/2}$$

$$p = g_{5/2}(z(T)) \left(\frac{2\pi m}{h^2} \right)^{3/2} (k_B T)^{5/2} \leftarrow \text{equation of state}$$

↑ for a system of fixed density n , z must be chosen to be a function of T that gives the desired density n .



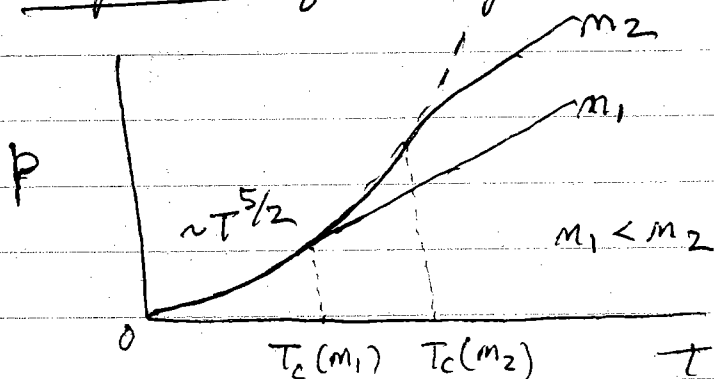
Note $g_{5/2}(z=1) = \zeta(5/2) = 1.342$
is finite

In thermodynamic limit of $V \rightarrow \infty$, $z=1$ for $T \leq T_c(n)$

$$\Rightarrow p = g_{5/2}(1) \left(\frac{2\pi m}{h^2} \right)^{3/2} (k_B T)^{5/2} \text{ for } T \leq T_c$$

↑ critical temperature depends on the system's fixed density

Note: for $T \leq T_c$, the pressure $p \propto T^{5/2}$ is independent of the system density!



p vs T curves at constant density n

recall $T_c(n) \sim n^{2/3}$

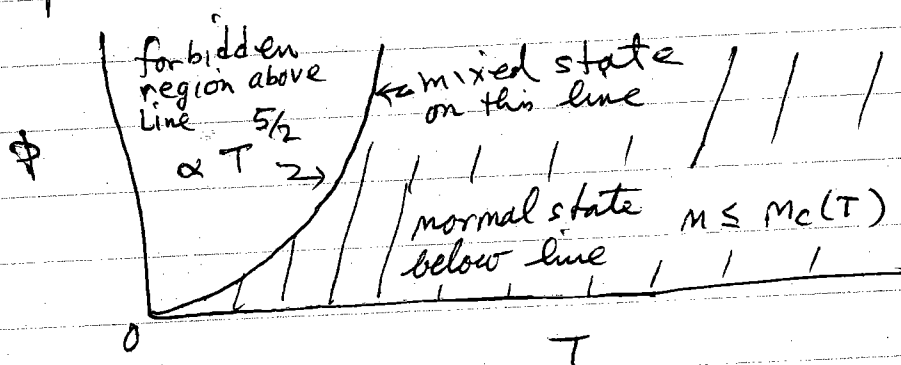
$$T_c(n) = \left(\frac{n}{2.16} \right)^{2/3} \frac{h^2}{2\pi m k_B}$$

Define $n_c(T) = 2.612 \left(\frac{2\pi m k_B T}{h^2} \right)^{3/2}$ inverse of $T_c(n)$

$n_c(T)$ is the critical density at a given T

— a system with $n > n_c(T)$ will be in a Bose condensed mixed state at temperature T .

phase diagram in p - T plane



Can also consider the transition in terms of p and $v = \frac{V}{N} = \frac{1}{n}$ for various fixed T .

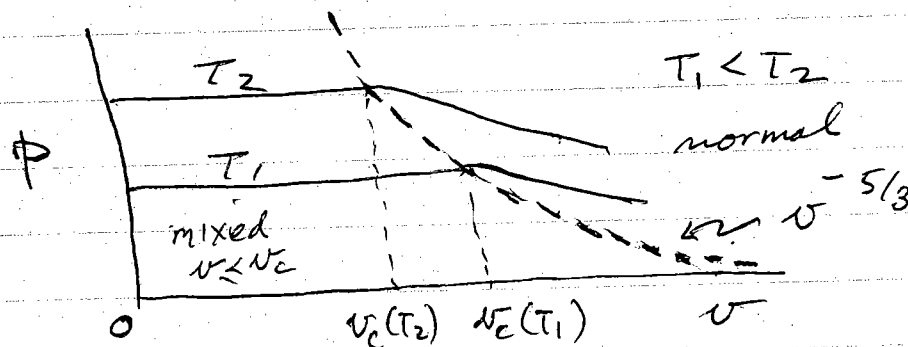
At the transition $p \propto T_c(n)^{5/2}$, $T_c(n) \propto n^{2/3}$

$\Rightarrow$ at the transition $p \propto (n^{2/3})^{5/2} = n^{5/3} = v^{-5/3}$

below the transition p is independent of density and hence independent of v .

For fixed T , the transition occurs when density n exceeds $n_c(T)$, or when v drops below $v_c(T) = \frac{1}{n_c(T)}$
 $v_c(T) \sim T^{-3/2}$

curves of p vs v at constant T



Thermodynamic functions

Earlier we found $\frac{E}{V} = \frac{3}{2} p$

$$\Rightarrow \frac{E}{N} = \frac{3}{2} p \frac{V}{N} = \frac{3}{2} p v = \frac{3}{2} \frac{k_B T v}{\lambda^3} g_{5/2}(z)$$

$z=1$ in mixed state
 $z < 1$ in normal state

In above we regard $\frac{E}{N}$ as a function of either v or z . That is we either determine v for a given z, T or we determine z needed for a given v, T (Recall $z = e^{\beta \mu}$, $v = \frac{V}{N}$ and N and μ are conjugate variables)

specific heat

$$\frac{C_V}{N k_B} = \frac{1}{k_B} \left(\frac{\partial (E/N)}{\partial T} \right)_{v, N} = \frac{3}{2} v \left\{ \frac{d}{dT} \left(\frac{T}{\lambda^3} \right) g_{5/2}(z) + \frac{T}{\lambda^3} \frac{\partial g_{5/2}(z)}{\partial z} \frac{dz}{dT} \right\}$$

For $T \leq T_c$, $z = 1$ so $\frac{dz}{dT} = 0$ and only 1st term remains

$$\frac{T}{\lambda^3} \propto T^{5/2} \text{ so } \frac{d}{dT} \left(\frac{T}{\lambda^3} \right) = \frac{5}{2} \left(\frac{T}{\lambda^3} \right) \frac{1}{T} = \frac{5}{2} \frac{1}{\lambda^3}$$

✓ $z=1$ here for all $T \leq T_c$

$$\begin{aligned} \Rightarrow \frac{C_v}{Nk_B} &= \frac{3}{2} \nu \left(\frac{5}{2} \frac{1}{\lambda^3} \right) g_{5/2}(1) = \frac{15}{4} g_{5/2}(1) \frac{\nu}{\lambda^3} \\ &= \frac{15}{4} g_{5/2}(1) \nu \left(\frac{2\pi m k_B T}{h^2} \right)^{3/2} \end{aligned}$$

Note, at T_c , $n = \frac{g_{3/2}(1)}{\lambda_c^3}$, and $\nu = \frac{1}{n}$

$$\frac{C_v(T_c)}{Nk_B} = \frac{15}{4} \frac{g_{5/2}(1)}{g_{3/2}(1)} = \frac{15}{4} \frac{1.341}{2.612} = 1.925$$

← this is larger than the classical ideal gas value of $\frac{3}{2}$

$$\text{So } \boxed{\frac{C_v}{Nk_B} = 1.925 \left(\frac{T}{T_c} \right)^{3/2} \quad T \leq T_c}$$

For $T \geq T_c$, z varies with T and we need to evaluate the 2nd term as well

↖ here z depends on T for $T > T_c$

$$\text{1st term gives } \frac{15}{4} g_{5/2}(z(T)) \frac{\nu}{\lambda^3}$$

2nd term: from Pathria Appendix D Eq(10),

$$z \frac{d}{dz} [g_\nu(z)] = g_{\nu-1}(z)$$

$$\Rightarrow \frac{d g_{5/2}}{dz} \frac{dz}{dT} = g_{3/2} \frac{1}{z} \frac{dz}{dT}$$

To find $\frac{1}{2} \frac{dz}{dT}$ consider our earlier result for the density when $T > T_c$:

$$n = \frac{g_{3/2}(z)}{\lambda^3} \quad \leftarrow \text{determines } z(T) \text{ for fixed } n$$

$$\text{for } n \text{ fixed} \Rightarrow 0 = \frac{dn}{dT} = \frac{d}{dT} \left(\frac{1}{\lambda^3} \right) g_{3/2} + \frac{1}{\lambda^3} \frac{dg_{3/2}}{dz} \frac{dz}{dT}$$

$$0 = \frac{3}{2} \frac{1}{\lambda^3 T} g_{3/2} + \frac{1}{\lambda^3} g_{1/2} \frac{1}{z} \frac{dz}{dT}$$

$$\Rightarrow \frac{1}{z} \frac{dz}{dT} = -\frac{3}{2} \frac{g_{3/2}}{g_{1/2}} \frac{1}{T}$$

$$\frac{C_V}{Nk_B} = \frac{15}{4} g_{5/2}(z) \frac{v}{\lambda^3} + \frac{3}{2} v \frac{T}{\lambda^3} g_{3/2}(z) \left(-\frac{3}{2} \right) \frac{g_{3/2}(z)}{g_{1/2}(z)} \frac{1}{T}$$

$$\text{use } n = \frac{1}{v} = \frac{g_{3/2}(z)}{\lambda^3} \Rightarrow \frac{v}{\lambda^3} = \frac{1}{g_{3/2}(z)}$$

$$\boxed{\frac{C_V}{Nk_B} = \frac{15}{4} \frac{g_{5/2}(z)}{g_{3/2}(z)} - \frac{9}{4} \frac{g_{3/2}(z)}{g_{1/2}(z)} \quad T > T_c}$$

$$\text{Note } g_{1/2}(1) = \sum_{\ell=1}^{\infty} \frac{1}{\ell^{1/2}} \rightarrow \infty$$

So as $T \rightarrow T_c^+$ from above, and $z \rightarrow 1$

$$\frac{C_V}{Nk_B}(T_c^+) = \frac{15}{4} \frac{g_{5/2}(1)}{g_{3/2}(1)} - \frac{9}{4} \frac{g_{3/2}(1)}{\infty} = \frac{15}{4} \frac{1.341}{2.612} = 1.925$$

$$\Rightarrow \boxed{C_V \text{ is continuous at } T_c}$$

Finally we want to show that although C_V is continuous at T_c , $\frac{dC_V}{dT}$ is discontinuous

For $T \leq T_c$ $\frac{C_V}{Nk_B} = 1.925 \left(\frac{T}{T_c} \right)^{3/2}$

$$\frac{d}{dT} \left(\frac{C_V}{Nk_B} \right) = \frac{3}{2} (1.925) \left(\frac{T}{T_c} \right)^{1/2} \frac{1}{T_c} = 2.89 \left(\frac{T}{T_c} \right)^{1/2} \frac{1}{T_c}$$

so slope at T_c^- (just below T_c)

w: $\boxed{\frac{d}{dT} \left(\frac{C_V}{Nk_B} \right) = \frac{2.89}{T_c}, \quad T = T_c^-}$

For $T > T_c$

$$\frac{C_V}{Nk_B} = \frac{15}{4} \frac{g_{5/2}(z)}{g_{3/2}(z)} - \frac{9}{4} \frac{g_{3/2}(z)}{g_{1/2}(z)}$$

$$\frac{d}{dT} \left(\frac{C_V}{Nk_B} \right) = \frac{15}{4} \frac{g_{3/2} \frac{dg_{5/2}}{dz} \frac{dz}{dT} - g_{5/2} \frac{dg_{3/2}}{dz} \frac{dz}{dT}}{(g_{3/2}(z))^2}$$

$$- \frac{9}{4} \frac{g_{1/2} \frac{dg_{3/2}}{dz} \frac{dz}{dT} - g_{3/2} \frac{dg_{1/2}}{dz} \frac{dz}{dT}}{(g_{1/2})^2}$$

$$= \frac{1}{z} \frac{dz}{dT} \left\{ \frac{15}{4} \left(\frac{g_{3/2}^2 - g_{5/2} g_{1/2}}{g_{3/2}^2} \right) - \frac{9}{4} \left(\frac{g_{1/2}^2 - g_{3/2} g_{-1/2}}{g_{1/2}^2} \right) \right\}$$

use $\frac{1}{z} \frac{dz}{dT} = -\frac{3}{2} \frac{g_{3/2}}{g_{1/2}} \frac{1}{T}$ as found earlier

$$\frac{d}{dT} \left(\frac{C_V}{Nk_B} \right) = -\frac{3}{8T} \frac{g_{3/2}}{g_{1/2}} \left\{ 15 \left(1 - \frac{g_{5/2} g_{1/2}}{g_{3/2}^2} \right) - 9 \left(1 - \frac{g_{3/2} g_{-1/2}}{g_{1/2}^2} \right) \right\}$$

Now as $T \rightarrow T_c^+$ from above, $z \rightarrow 1$, we have

$g_{5/2}(1)$ and $g_{3/2}(1)$ are finite, but $g_{1/2}(1)$ and $g_{-1/2}(1) \rightarrow \infty$

$\Rightarrow$ at T_c^+

$$\frac{d}{dT} \left(\frac{C_V}{Nk_B} \right) = \frac{45}{8T_c} \frac{g_{5/2}(1)}{g_{3/2}(1)} - \frac{27}{8T_c} \frac{g_{3/2}(1)^2}{g_{1/2}(1)^3} g_{-1/2}(1)$$

Now from Pathria Appendix D Eq(8)

$$g_\nu(1) = \lim_{a \rightarrow 0} \frac{\Gamma(1-\nu)}{a^{1-\nu}}$$

$$\text{So } \frac{g_{-1/2}(1)}{g_{3/2}(1)} = \lim_{a \rightarrow 0} \frac{\Gamma(3/2)}{a^{3/2}} \left(\frac{a^{1/2}}{\Gamma(1/2)} \right)^3 = \frac{\Gamma(3/2)}{[\Gamma(1/2)]^3}$$

$$= \frac{\frac{1}{2} \pi^{1/2}}{\pi^{3/2}} = \frac{1}{2\pi} \quad \text{since } \Gamma(1/2) = \sqrt{\pi} \\ \Gamma(3/2) = \frac{1}{2} \sqrt{\pi}$$

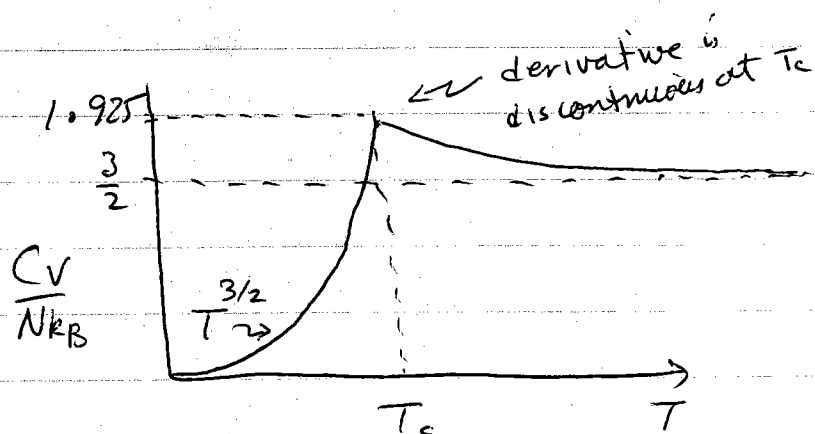
$$\frac{d}{dT} \left(\frac{C_V}{Nk_B} \right) = \frac{45}{8} \frac{1.341}{2.612} \frac{1}{T_c} - \frac{27}{8} \frac{(2.612)^2}{2\pi} \frac{1}{T_c}$$

$$= \frac{2.89}{T_c} - \frac{3.66}{T_c} = -\frac{0.77}{T_c}$$

$$\boxed{\frac{d}{dT} \left(\frac{C_V}{Nk_B} \right) = -\frac{0.77}{T_c}, \quad T = T_c^+}$$

slope of C_V
is discontinuous at
 T_c .

C_V has a cusp at T_c



goes to classical $\frac{3}{2}$ as $T \rightarrow \infty$

$$\frac{dC_V}{dT} > 0 \quad \text{for } T = T_c^-$$

$$\frac{dC_V}{dT} < 0 \quad \text{for } T = T_c^+$$

Entropy

For single species gas we had for Gibbs free energy

$$G = N\mu$$

$$\text{Also } G = E - TS + pV$$

(since G is Legendre transform E with respect to S and V)

$$\Rightarrow N\mu = E - TS + pV$$

$$\text{or } S = \frac{E + pV - N\mu}{T}$$

$$\frac{S}{Nk_B} = \frac{E + pV}{Nk_B T} - \frac{\mu}{k_B T}$$

$$\text{we had earlier } E = \frac{3}{2} pV \Rightarrow pV = \frac{2}{3} E$$

$$\frac{S}{Nk_B} = \frac{5}{3} \frac{E}{N} \frac{1}{k_B T} - \frac{\mu}{k_B T}$$

$$z = e^{M/k_B T}, \quad z = 1 \text{ for } T < T_c$$

we had earlier $\frac{E}{N} = \frac{3}{2} \frac{k_B T}{\lambda^3} g_{5/2}(z)$

and $n = \frac{1}{v} = \frac{g_{3/2}(z)}{\lambda^3}$ for $T > T_c$

$$\Rightarrow \frac{S}{N k_B} = \frac{5}{2} \frac{v}{\lambda^3} g_{5/2}(z) - \ln z = \begin{cases} \frac{5}{2} \frac{g_{5/2}(z)}{g_{3/2}(z)} - \ln z, & T > T_c \\ \frac{5}{2} \frac{v}{\lambda^3} g_{5/2}(1), & T \leq T_c \end{cases}$$

Note: For $T \leq T_c$ we had that the density of the "normal" a density $m_0 = n - \frac{g_{3/2}(1)}{\lambda^3}$ in

the condensate, and a density $\frac{g_{3/2}(1)}{\lambda^3}$ in the "normal" state (i.e. the density of excited particles) $\frac{g_{3/2}(1)}{\lambda^3} \equiv m_n$

$$\Rightarrow \text{for } T \leq T_c, \quad \frac{S}{N k_B} = \frac{5}{2} \left(\frac{m_n}{m} \right) \frac{g_{5/2}(1)}{g_{3/2}(1)} \rightarrow 0 \text{ as } T \rightarrow 0$$

we can imagine that each normal particle carries entropy $\frac{5}{2} k_B \frac{g_{5/2}(1)}{g_{3/2}(1)}$. The entropy at $T < T_c$ /per particle

is just the ~~fact~~ above entropy per "normal" particle times the fraction of normal particles.

$\Rightarrow$ normal particles carry the entropy
condensate has zero entropy

entropy difference per particle between normal state and condensed state is $\frac{\Delta S}{N} = \frac{5}{2} k_B \frac{g_{5/2}(1)}{g_{3/2}(1)}$

latent heat of condensation

$$L = T \Delta S = \frac{5}{2} k_B T \frac{g_{5/2}(1)}{g_{3/2}(1)}$$

energy released upon converting one normal particle to one condensate particle.

$\Rightarrow$ mixed phase is like coexistence region of a 1st order phase transition (like water $\leftrightarrow$ ice $\frac{3}{2}$ - need to remove energy to turn water to ice)

$\Rightarrow$ "two fluid" model of mixed region

The existence of Bose Einstein condensation is particular to the dimensionality of the system. To see this, consider a general d -dimensional system. Then

$$\frac{1}{V} \sum_k n(\epsilon(k)) \rightarrow \propto \int d^d k \, k^{d-1} \frac{1}{z^{-1} e^{\beta \hbar^2 k^2 / 2m} - 1}$$

is largest when $z \rightarrow 1$, so consider this case

$$\propto \int d^d k \, k^{d-1} \frac{1}{e^{\beta \hbar^2 k^2 / 2m} - 1}$$

$$\text{let } y = \frac{\beta \hbar^2 k^2}{2m}$$

$$k = \sqrt{\frac{2m y}{\beta \hbar^2}}$$

$$dk = \sqrt{\frac{2m y}{\beta \hbar^2}} \frac{dy}{2y}$$

$$\propto \left(\frac{2m}{\beta \hbar^2}\right)^{d/2} \int_0^\infty dy \frac{y^{\frac{d}{2}-1}}{e^y - 1}$$

again the most singular part of the integral is as $y \rightarrow 0$

$$\text{for } y^* \ll 1, \quad \int_0^{y^*} dy \frac{y^{\frac{d}{2}-1}}{e^y - 1} \approx \int_0^{y^*} dy \frac{y^{\frac{d}{2}-1}}{y} = \int_0^{y^*} dy \, y^{\frac{d}{2}-2}$$

The integral will converge at its lower limit $y \rightarrow 0$

only for $\frac{d}{2} - 2 > -1$ or $d > 2$

For $d \leq 2$, the integral will diverge. Therefore it will always be possible to find a z such that

$$n = \frac{N}{V} = \frac{1}{(2\pi)^d} \int d^d k \frac{1}{z^{-1} e^{\beta \hbar^2 k^2 / 2m} - 1}$$

$\Rightarrow$ No Bose Einstein Condensation in two dimensions or below.